Effects of Graphene Nanoplatelets and Multiwall Carbon Nanotubes on the Structure and Mechanical Properties of Poly(lactic acid) Composites: A Comparative Study

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Abstract: Poly(lactic acid)/graphene and poly(lactic acid)/carbon nanotube nanocomposites were prepared by an easy and low-cost method of melt blending of preliminary grinded poly(lactic acid) (PLA) with nanosized carbon fillers used as powder. Morphological, structural and mechanical properties were investigated to reveal the influence of carbon nanofiller on the PLA–based composite. The dependence of tensile strength on nanocomposite loading was defined by a series of experiments over extruded filaments using a universal mechanical testing instrument. The applying the XRD technique disclosed that compounds crystallinity significantly changed upon addition of multi walled carbon nanotubes. We demonstrated that Raman spectroscopy can be used as a quick and unambiguous method to determine the homogeneity of the nanocomposites in terms of carbon filler dispersion in a polymer matrix.

Keywords: nanocomposites; carbon nanofillers; poly(lactic) acid (PLA); tensile strength; structure properties

1. Introduction

Last decade, many scientific efforts have been made for the synthesis of multifunctional polymer nanocomposites that take advantage of the unique mechanical and structural properties of new graphitic forms as graphene (GNPs) and multiwall carbon nanotubes (MWCNTs) [1–5]. There are a lot of studies on carbon composites based on a wide range of polymers, reported in the literature as polycarbonate [6], nylon [7], poly(methyl methacrylate) [8], epoxy resin [9], poly(vinyl alcohol) [10], polystyrene [11], polycaprolactone [12], poly(propylene) [13], and poly(lactic acid) [14,15]. One of the main parameters that influences the composite properties is the distribution/dispersion of the carbon nanofillers in conjunction with their weight percentage loading in the polymer matrix [16,17]. X-ray diffractometry (XRD), as a safe method of nanocomposite characterization, has been used to reveal
information on the existence of GNPs in the form of individual graphene sheets in epoxidized palm oil blends [18], to disclose the effect of sonication time on the dispersion ability of graphene in the PLA matrix [19], to confirm intactness and reliable distribution of reduced graphene oxide (rGO) as graphene sheet layers into a polymer composite [20], and to study the influence of carbon nanofiller on the semi-crystalline structure of PLA and PBAT [21]. Abdal-Hay et al. [22] reported that PLA and nanocomposites containing different CNT concentrations exhibited nearly the same diffraction peaks at slightly different locations.

Raman spectroscopy provides molecular morphology analysis, giving information on the composite material structure by evaluation of relevant vibrational features and could be used to characterize the degree of graphene or nanotube dispersion. Bounos et al. [23] investigated MWCNT loading, excitation laser power and temperature as parameters affecting the frequency of the Raman bands and their intensity. They reported that in the specific case of isotactic polypropylene (iPP), any interaction of the carbon nanotubes with the polymeric host has minimal effect on the frequency of the MWCNT’s G band (~1584 cm\(^{-1}\)); the same holds for the influence of residual stresses acting on the MWCNTs. The parameter that primarily altered the CNT’s Raman bands frequency was temperature, determined by the excitation laser intensity, the MWCNTs concentration and the thermal properties of the polymer matrix. This was demonstrated by confocal micro-Raman spectra collected from agglomerates and from micro-Raman spectra of samples containing either poorly or well dispersed MWCNTs.

Raman confocal spectroscopy has been used for characterization of MWCNTs embedded in PLA fibers in the absence of a chemical interaction between them [24]. By means of confocal images, agglomerates of carbon nanotubes have been noticed, even after solution ultrasound sonication. The Raman spectrum of MWCNTs, as expected, showed the graphitic D, G and G’ bands at 1362, 1590 and 2683 cm\(^{-1}\), respectively.

In a recent article [26], the influence of filler size on the properties of poly(lactic acid) (PLA)/graphene nanoplatelets (GNP) nanocomposites were investigated. Morphological, thermal, mechanical, and electrical properties were studied to reveal the influence of particle size. Electron microscopy and X-ray diffraction showed well dispersed small GNP (GNP-S) particles up to 10 wt% loading, while large GNP (GNP-L) particles started to agglomerate at loadings ≥7 wt%. Notably, composites with GNP-L demonstrated a much stronger peak than those with GNP-S at the same loading, indicating that large GNP-L fillers induce higher polymer crystallinity than small GNP-S in the composites. The XRD results also demonstrated that there is no significant change in PLA crystallinity with the incorporation of both GNP types, regardless of their size.

X-ray powder diffraction analyses were carried out over polylactide (PLA)/graphene nanocomposites, prepared by a facile and low-cost method of solution blending of PLA with liquid-phase exfoliated graphene using chloroform as a mutual solvent [27]. The dispersion of graphene in a PLA matrix has been examined by physical methods as SEM, XRD and TEM. The authors reported that the XRD pattern of PLA-based nanocomposites loaded with 0.1 wt% graphene sheets (GSs) was almost the same as that of pure PLA, in which two characteristic diffraction peaks are shown at 16.3 and 18.7°, corresponding to (200)/(110) and (203) planes of crystalline PLA, respectively. The diffraction peak at 26° corresponding to graphite layer structure (002) was not observed in GSs due to the exfoliation. The scattering intensity profile did not reveal the presence of the diffraction
peak of graphite, suggesting that the GSs do not aggregate in a PLA matrix. As suggested by some authors, this result indicates that the dispersion of GSs in a PLA matrix is close to single-sheet level.

In another paper [28], D. Singh et al. made research over the diameter dependence of interwall separation and strain in multiwalled carbon nanotubes probed by X-ray diffraction and Raman scattering studies. The authors did a systematic study on the diameter dependent spectral features in X-ray diffraction (XRD) and Raman scattering studies of multiwalled carbon nanotubes (MWCNTs) of various diameters in the range 5–100 nm. Analysis of the XRD patterns showed an exponential decrease in \(d_{002}\) interlayer spacing with increasing tube diameter, in close agreement with the HRTEM results. Analysis of Raman and XRD data disclosed that the lowest diameter (7 nm) MWCNTs have features similar to those of the single walled nanotubes, while the spectral features are distinctly different for higher diameter MWCNTs.

Relationships between structure and properties of nanocomposite materials can be made through a combination of structural investigations (such as Raman spectroscopy and X-ray diffraction) and mechanical tests in order to have better understanding of these nanocomposites. The effects of increasing filler content on the macro-mechanical properties of polymer nanocomposites can be investigated through tensile, flexural or impact tests. Some previous results for mechanical properties of PLA reinforced with carbon nanostructures as graphene [29,30], carbon nanotubes [31] and both nanofillers [32] have been reported in the literature. The incorporation of carbon fillers in a polymer matrix is expected to improve the mechanical properties, especially when carbon nanotubes are used as a reinforcing material [33].

The aim of the present study was to estimate the influence of two different carbon nanofillers and the relevant loading amount on the structure and homogeneity of PLA-based nanocomposites. Another challenge was to elucidate the dispersion degree of both carbon nanofillers at all composites loadings, as well as to study the effect of GNP and MWCNTs on the crystal structure of PLA (at high filler contents). The novelty in this study is related to an important detail in the preparation method consisting of preliminary grinding of PLA and then using PLA as a powder during melt mixing of the polymer with the carbon nanofiller.

2. Materials and Methods

2.1. Materials

Ingeo™ Biopolymer PLA-3D850 (Nature Works) with MFR 7–9 g/10 min (210 °C, 2.16 kg) and \(M_w \sim 60000\) g/mol was purchased from Nature Works, Minnetonka, MN, USA.

MWCNT (NC7000, from Nanocyl, Sambreville, Belgium): Diameter (OD) 9.5 nm; Length 1.5 \(\mu\)m, Purity 90%; Specific surface area \(SSA = 250–300\) \(m^2/g\); Volume resistivity \(10^{-4}\) \(\Omega\cdotcm\) and TNGNP (Graphene Nanoplatelets, TimesNano, Chengdu, China) – average thickness < 4–20 nm and diameter of ~5–10 \(\mu\)m; Purity 99.5%; Volume Resistivity \(4 \times 10^{-4}\) \(\Omega\cdotcm\) were supplied from TimesNano, Chengdu, China.

2.2. Preparation of Nanocomposites

The compounds were made by means of the melt extrusion technique. The PLA pellets were grinded and then used as powder. Mono-filler nanocomposites were synthesized that way, containing graphene or carbon nanotubes and having filler content from 0 to 9 wt%. All produced and tested compounds are listed in Table 1.
Table 1. List of PLA-based nanocomposites.

<table>
<thead>
<tr>
<th>No.</th>
<th>Sample Index</th>
<th>PLA Content (wt%)</th>
<th>MWCNT Content (wt%)</th>
<th>GNP Content (wt%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>1.5GNP/PLA</td>
<td>98.5</td>
<td>-</td>
<td>1.5</td>
</tr>
<tr>
<td>2</td>
<td>3GNP/PLA</td>
<td>97</td>
<td>-</td>
<td>3</td>
</tr>
<tr>
<td>3</td>
<td>6GNP/PLA</td>
<td>94</td>
<td>-</td>
<td>6</td>
</tr>
<tr>
<td>4</td>
<td>9GNP/PLA</td>
<td>91</td>
<td>-</td>
<td>9</td>
</tr>
<tr>
<td>5</td>
<td>1.5MWCNT/PLA</td>
<td>98.5</td>
<td>1.5</td>
<td>-</td>
</tr>
<tr>
<td>6</td>
<td>3MWCNT/PLA</td>
<td>97</td>
<td>3</td>
<td>-</td>
</tr>
<tr>
<td>7</td>
<td>6MWCNT/PLA</td>
<td>94</td>
<td>6</td>
<td>-</td>
</tr>
<tr>
<td>8</td>
<td>9MWCNT/PLA</td>
<td>91</td>
<td>9</td>
<td>-</td>
</tr>
<tr>
<td>9</td>
<td>PLA</td>
<td>100</td>
<td>-</td>
<td>-</td>
</tr>
</tbody>
</table>

2.3. Preparation of Test Samples

Circular cross-section samples with a diameter of about 1.75 mm and length of 5 cm were cut from extruded filaments and then applied for tensile tests. The samples needed for Raman and XRD analysis were hot pressed with a thickness of ~1 mm and diameter of 20 mm.

2.4. Experimental Methods

Two types of monofilled nanocomposites (MWCNT/PLA and GNP/PLA) were used for a series of tensile tests in order to evaluate the material’s mechanical characteristics. The experiments were carried out on UMT–2 Universal Tester modular system (Bruker, Billerica, MA, USA) developed by Bruker. Tensile tests were performed by using a 1–100 kg (1000 N) force sensor. The set tensile speed was 1 mm/min at room temperature. The standard error was determined by testing 7 samples of each composition. During the experiment, the working section of the sample under tension was exactly 1 cm.

The KBr technique was applied for determining the FT-IR spectra of the samples, in the scanning range from 4000 to 400 cm\(^{-1}\), by using a Vertex 70 instrument (Bruker Corporation).

Single spectra were taken on an inVia confocal Raman microscope spectrometer Renishaw, using a 50x excitation green argon ion laser with 1800 L/mm grating. The power radiation was 12.5 mW at 514 nm wavelength edge laser physics and 10 seconds integration time. A laser beam with a diameter of approximately 2.5 \(\mu\)m was focused onto the surface of each nanocomposite sample.

X-ray powder and nanocomposite diffraction (XRD) analyses were carried out on a Bruker D8 Advance diffractometer (Billerica, MA, USA) at 40 kV and 40 mA with Cu K\(\alpha\) radiation (\(\lambda = 0.15418 \text{nm}\)), and the diffraction data were recorded for 20 angles between 0\(^{\circ}\) and 50\(^{\circ}\) applying a scanning rate of 4\(^{\circ}\) min\(^{-1}\).

The morphology of the nanocomposites was observed by a field emission scanning electron microscope (FESEM, mod. LEO 1525, Carl Zeiss SMT AG, Oberkochen, Germany). Hot pressed samples were immersed in liquid nitrogen, then cut to get the cross-section and finally coated with gold (layer thickness 250 \(\AA\)) using a sputter coater (mod. B7341, Agar Scientific, Stansted, UK).

3. Results and Discussion

3.1. Infrared Spectroscopy Analysis

In the IR-spectrum of GNP, bands corresponding to stretching vibrations of CH group at 2853 \(\text{cm}^{-1}\) and 2920 \(\text{cm}^{-1}\) could be observed (see Figure 1). The bands at 3444 \(\text{cm}^{-1}\), at 1649 \(\text{cm}^{-1}\) and 1109 \(\text{cm}^{-1}\) are due to stretching vibrations of the \(-\text{OH}, \ C=O\) and \(\text{C–O}\) adsorption groups. Overall, these bands, which are typical of non-functionalized materials [34], indicate that GNP’s contain defects.
Appl. Sci. 2019, 9, 469

Figure 1. IR spectrum of GNPs.

The IR spectrum of carbon nanotubes (Figure 2), showed intense bands corresponding to stretching vibrations of –OH, C=O and C–O, together with new bands corresponding to carboxyl groups (–COOH): ν(C=O) at 1741 cm⁻¹ and C=O bond at 1028 cm⁻¹, indicating a MWCNTs surface functionalization. These typical bands, with slight variations in wavelength, can be found for carbon nanotube oxidized in different ways [35].

Figure 2. IR spectrum of multi walled carbon nanotubes.

3.2. Raman Analysis

Raman spectroscopy has become a standard characterization tool for carbon nanostructures [36–39]. Tensile, compressive and shear stress applied to carbon nanotubes induce strain, leading to changes in the C–C bond vibrations, which strongly affect the Raman spectrum [40]. Stress induced changes in peak positions and intensities have been observed for individual carbon nanotubes [41], SWCNT bundles [42] and nanotube–polymer composites [43]. Normalized Raman spectra of the nanocomposites with increasing MWCNTs and GNP's concentration including pristine nanofiller as a reference are depicted in Figures 3 and 4. In all single spectra, the main Raman bands—G, D and 2D, or also denoted as G', band have been registered. The 1582 cm⁻¹ band of graphene is known as the G band or tangential band and originates from in-plane vibration of sp² carbon atoms. The band at about 2700 cm⁻¹, which is recognized as the G' or 2D band, is much more intense than the G band in graphene compared to graphite or to multilayer graphene. This band is a second-order overtone mode and does not represent a disorder-induced mode. The 2D band has frequently been used to study MWCNT-polymer interfacial stress transfer. The 2D peak is an overtone of the D band, resulting from a two-phonon double-resonant Raman process [44]. The D band at around 1350 cm⁻¹ is often referred as disorder band or defect band and its intensity relative to the G
band intensity is often used as a measure of carbon nanotubes quality. All Raman results concerning monofilier PLA-based nanocomposites are summarized in Figures 3 and 4, and Table 2.

The presence of MWCNTs in the composites is supported by the characteristic D, G, and 2D modes of MWCNTs (Figure 3). D, G, and 2D modes of the MWCNT/PLA composites exhibit positional upshift, more pronounced in the 2D band, as compared to the pure MWCNTs itself. Shifts to higher-frequencies, especially for the G band, have been reported in MWCNTs composites [45]. This blue shift has been attributed to a disentanglement and dispersion of the CNT bundles in the polymer matrix, decreasing nanotube-nanotube interactions. The application of a deformation to CNTs results in a change in the C–C bond vibrations, leading to a change in the vibrational frequencies of the normal modes and thus to Raman band shifts. Strain-induced frequency changes have been already reported for MWCNTs composites [43]. In terms of the relative Raman intensity, evaluated against the G mode intensity, and the full width at half maximum intensity (FWHM), we can observe different distinct behaviors: the D intensity decreased substantially upon rising carbon nanotube content in the composite, whereas the 2D mode exhibits a cutback of the relative intensity as well as a significant reduction of FWHM. These changes can be due to the interaction between PLA and carbon nanotubes. It is worth noticing, that the resonances of pure PLA, due to C–CH₃ stretching at about 1042 cm⁻¹ and –CH₃ rocking mode at about 1127.4 cm⁻¹, were red-shifted by 2.1, 1.3, and 1.8 cm⁻¹ in the Raman spectrum of 3 wt% MWCNT/PLA composite regarding the spectrum of 1.5 wt% MWCNT/PLA composite, indicating that the interaction of MWCNTs with the polymer occurs through C–CH₃ groups [46,47], see Figure 3b.

![Normalized Raman spectra of nanocomposites with rising MWCNTs concentration and pristine nanotubes as a reference (a), enlargement between 1000 and 1500 cm⁻¹ (b).](image_url)

**Figure 3.** Normalized Raman spectra of nanocomposites with rising MWCNTs concentration and pristine nanotubes as a reference (a), enlargement between 1000 and 1500 cm⁻¹ (b).

As already mentioned, the 2D band of the nanocomposites in Figure 3 is barely shifted to higher Raman frequencies, compared with the 2D band of pure carbon nanotubes. A possible reason for this could be as well the relatively low filler concentration in the polymer matrix compared to the neat MWCNTs [23]. When the carbon nanotubes are multi walled, their diameter becomes larger, so the lattice strain is reduced, leading to a decline in the number of sp³ hybridized carbon, which means the tubular structure is not so stable [28]. The weak blueshift of the G band at 6 wt% and 9 wt% MWCNT loadings could be understood in terms of the strain effect caused by the interaction between carbon nanotubes and the PLA matrix.
As the number of graphitic layers increases, the interaction between these layers becomes significant, reflecting in the appearance of a shoulder over the 2D band in the Raman spectra of GNP/PLA nanocomposites (Figure 4). This shoulder shifts the position of the 2D band to the higher frequencies of the spectrum. Concerning graphene samples, the small differences in the G band position up to 3 cm$^{-1}$ (1575–1578 cm$^{-1}$) are suggested to be within the range of fluctuations caused by unintentional electron or hole doping effects [48]. It was found that the influence of the PLA structure on the Raman spectra of the nanocomposites decreases with rising carbon filler loading.

The $I_{2D}/I_G$ ratio shows the graphene quality. Regarding high quality defect-free graphene, this ratio will be equal to 2 (single or few layers graphene). The defined $I_{2D}/I_G$ ratios of TNGNP and GNP/PLA nanocomposites are rather a hint for the presence of multilayer graphene in the composite structure (Table 2). Mapping Raman analysis was carried out on each sample, acquiring spectra at least on three surface sample positions, in order to have a better picture of nanocomposite homogeneity.

![Figure 4. Normalized Raman spectra of nanocomposites with growing GNPs concentration and pristine graphene as reference.](image)

Table 2. Raman intensities ratios of monofiller nanocomposites.

<table>
<thead>
<tr>
<th>Sample</th>
<th>$I_D/I_G$ (±)</th>
<th>$I_{2D}/I_G$ (±)</th>
</tr>
</thead>
<tbody>
<tr>
<td>TNGNP</td>
<td>0.10 ± 0.01</td>
<td>0.45 ± 0.01</td>
</tr>
<tr>
<td>MWCNT_Nanocyl</td>
<td>1.00 ± 0.01</td>
<td>0.55 ± 0.02</td>
</tr>
<tr>
<td>1.5MWCNT/PLA</td>
<td>1.14 ± 0.03</td>
<td>0.50 ± 0.01</td>
</tr>
<tr>
<td>3MWCNT/PLA</td>
<td>0.85 ± 0.03</td>
<td>0.33 ± 0.02</td>
</tr>
<tr>
<td>6MWCNT/PLA</td>
<td>0.71 ± 0.02</td>
<td>0.14 ± 0.01</td>
</tr>
<tr>
<td>9MWCNT/PLA</td>
<td>0.72 ± 0.005</td>
<td>0.12 ± 0.01</td>
</tr>
<tr>
<td>1.5GNP/PLA</td>
<td>0.30 ± 0.06</td>
<td>0.63 ± 0.03</td>
</tr>
<tr>
<td>3GNP/PLA</td>
<td>0.18 ± 0.04</td>
<td>0.50 ± 0.04</td>
</tr>
<tr>
<td>6GNP/PLA</td>
<td>0.15 ± 0.002</td>
<td>0.49 ± 0.03</td>
</tr>
<tr>
<td>9GNP/PLA</td>
<td>0.11±0.02</td>
<td>0.48±0.04</td>
</tr>
</tbody>
</table>

Peaks ratio calculations disclosed that even the pristine GNP and MWCNT are not fully homogeneous. However, a high level of homogeneity occurred in the nanocomposites. That was confirmed by the low standard deviations in the $I_D/I_G$ and $I_{2D}/I_G$ ratios for each sample, showing a high level of homogeneity in the nanocomposites structure (see Table 2). The fewer lattice defects led to a lower $I_D/I_G$ value. An indication of the low amount of structural defects in MWCNT/PLA nanocomposites is the narrow $I_D/I_G$ ratio, mostly concerning the higher MWCNTs loadings that could
signify good dispersion of carbon nanotubes in the polymer matrix. The peak intensity ratios $I_D/I_G$ of graphene nanocomposites are slightly higher than that of TNGNP, suggesting the formation of more basal plane and edge defects in the carbon filler present in GNP/PLA that could enhance the interface interactions in the composite. Nevertheless the low $I_D/I_G$ values of GNP/PLA nanocomposites, really close to the $I_D/I_G$ ratio of pure graphene nanoplatelets, can be an indication that the structure of GNP has been well preserved during melt extrusion processing. The standard deviations for all $I_D/I_G$ and $I_{2D}/I_G$ ratios have been taken into consideration when presenting the data in Table 2.

3.3. XRD Analysis

Pristine graphene exhibits a basal reflection (002) sharp peak at $2\theta = 27.0^\circ$ corresponding to a $d$ spacing of 3.370 Å in graphite layer structure (Figure 5). The graphene showed a more intensive peak than the carbon nanotubes pattern at $2\theta = 26.26^\circ$, indicating a more crystalline structure for GNP. Considering the spectral profile of MWCNT, the weak broad XRD peak at $2\theta = 43.54^\circ$ is assigned to graphitic (100) crystalline lattice.

A broad amorphous peak was observed as result of neat PLA XRD analysis at around $20.0^\circ$ combined with a weak sharp peak appearing at $17.2^\circ$ (Figure 6). This is an indication of scattering in the polymer matrix and confirms that the neat PLA has a partially pseudo orthorhombic α crystalline structure with a left handed 10/3 helices chain conformation but predominantly it is a biodegradable polymer possessing an amorphous microstructure. The analysis of the patterns in Figure 6 is evidence that the intensity of the GNPs (002) peak increases with increasing GNPs loading in PLA, as expected. Regarding the XRD analysis of the 9 wt% GNP/PLA composite, a distinct diffraction is observed at $27.2^\circ$, relating to an interlayer spacing of 0.33 nm, based on the Bragg’s law, which is associated with the graphitic (002) plane. On the other hand, the position change indicates that the spacing between graphene nanoplatelets in the composites shortened (from an interlayer spacing of 0.34 nm of 6 wt% GNP/PLA to 0.33 nm for 9 wt% GNP/PLA based on Bragg’s law). The addition of GNPs affects the semi-crystalline structure of the polymer: the crystalline PLA peak at $2\theta\sim 17.2^\circ$ in PLA/GNP nanocomposites is absent.

Figure 5. XRD patterns of pure graphene and carbon nanotubes.
The disappearance of PLA crystallinity with growing graphene content can be explained as a result of interfacial effects influencing the PLA semi-crystalline structural order. The XRD technique could provide information about the stacking thickness of the GNP crystallites. The average pristine nanoplatelet thickness as well as the size of the incorporated graphene was calculated by using the Scherrer equation. It was found that pure GNP has a thickness of about ~80 nm. This dimension remains roughly the same in the composite having 9 wt% GNP (~82 nm).

The high intensity recorded at 9 wt% GNP loading could be attributed to a relatively intense number of graphene layers organized in stacks. The X-ray diffraction of 6 wt% GNP/PLA nanocomposites revealed a less intensive graphite (002) pattern and weak feature of the broad PLA peak. The disappearance of PLA crystallinity with growing graphene content can be explained as a result of interfacial effects influencing the PLA semi-crystalline structural order. The XRD technique could provide information about the stacking thickness of the GNP crystallites. The average pristine nanoplatelet thickness as well as the size of the incorporated graphene was calculated by using the Scherrer equation. It was found that pure GNP has a thickness of about ~80 nm. This dimension remains roughly the same in the composite having 9 wt% GNP (~82 nm).

The influence of the carbon nanotubes loading on the polymer crystallinity is prominent in Figure 6. X-ray diffraction of nanocomposites with rising carbon nanotubes concentration and neat PLA as a reference.

The intensity recorded at 9 wt% GNP loading could be attributed to a relatively intense number of graphene layers organized in stacks. The X-ray diffraction of 6 wt% GNP/PLA nanocomposites revealed a less intensive graphite (002) pattern and weak feature of the broad PLA peak. The disappearance of PLA crystallinity with growing graphene content can be explained as a result of interfacial effects influencing the PLA semi-crystalline structural order. The XRD technique could provide information about the stacking thickness of the GNP crystallites. The average pristine nanoplatelet thickness as well as the size of the incorporated graphene was calculated by using the Scherrer equation. It was found that pure GNP has a thickness of about ~80 nm. This dimension remains roughly the same in the composite having 9 wt% GNP (~82 nm).

The influence of the carbon nanotubes loading on the polymer crystallinity is prominent in Figure 7. X-ray diffraction of nanocomposites with rising carbon nanotubes concentration and neat PLA as a reference.

The influence of the carbon nanotubes loading on the polymer crystallinity is prominent in Figure 7. The improvement of the sharp PLA peak at about 17.0° is more significant for the compound
loaded with 9 wt% MWCNT and less intense for the composite possessing 3 wt% MWCNT. Both composite diffraction patterns are an indication of more crystalline structure compared to the neat PLA. Graphitic (002) and (100) patterns are visible mostly for the 9 wt% MWCNT/PLA composite, which could be a sign of good carbon nanotube dispersion in the polymer matrix. This behavior, which shows a different trend compared to that of GNP, can be attributed to the dimensionality of the nanoparticles and probably also to the different degree of functionalization of the nanocarbons, where carboxyl groups can act as crystallinity centers in the polymer matrix. Indeed, nanofillers are reported to act in nucleating in nanocomposites [49], with crystalline layers covering the filler [50]. On the other hand, functional groups can improve crystallization [51], indeed only one nucleating site is needed, for the polymer, to start crystallization. Moreover, polymer chains crystalline formation continues more easily on different nanoparticle dimensionalities, which can influence the crystallization behavior of the polymer, (i.e. the polymer chains align along the nanofiller surface) [52].

3.4. Tensile Test Analysis

There are three possible types of interactions for composites that have nanofiller in their structure (polymer–nanofiller, nanofiller–nanofiller, and interface–polymer interactions), but the mechanism and the magnitude of the load transfer between polymer matrices and the nanofiller are still unclear concerning mechanical properties.

Considering the influence of carbon nanofillers on the macromechanical properties of nanocomposites, the main and most important tensile mechanical characteristics; ultimate (tensile) strength, elongation at ultimate strength and Young’s modulus, have been compared. The dependence of ultimate strength as a function of filler content in MWCNT/PLA and GNP/PLA nanocomposites is shown in Figure 8a.

![Figure 8](image)

**Figure 8.** Tensile strength (a) and elongation at ultimate strength (b) vs. carbon filler content for MWCNT/PLA and GNP/PLA nanocomposites.

The nanocomposites possessing GNP in the PLA matrix exhibit a trend of a slight decrease in ultimate strength as well as in elongation at a break when increasing the content filler. A possible reason for this could be a poor dispersion of graphene in the polymer volume and/or changes in polymer crystallinity due to the nanoparticles addition. The character of the curve describing nanocomposites with MWCNT/PLA is quite different. The incorporation of MWCNT significantly raises the tensile strength and elongation at ultimate strength parameters up to 6 wt% carbon filler content, see Figure 8. Above a 20% increase in the tensile strength of the MWCNT/PLA composite is observed at 6 wt% carbon nanotubes content compared to the neat PLA. The rising of carbon nanotubes loading from 1.5 wt% to 6 wt% enhances the elongation at ultimate strength, as can be seen in Figure 8b. This is due to the interfacial polymer-filler interaction related to the distinct hybrid structure between MWCNT
and polymer chains. The lower values of ultimate strength and elongation at ultimate strength for 9 wt% MWCNT/PLA nanocomposites could be explained by the high carbon nanotube concentration making the composite too crumbly and resulting in worst macromechanical properties.

Young’s modulus as a function of carbon filler content for both studied monofiller composite materials is presented in Figure 9. An insignificant impact has been observed concerning the nanocomposite elasticity by adding GNP in a PLA matrix. The Young’s modulus is increasing in the case of carbon nanotubes loading up to 9 wt% filler content. The higher elasticity that could be seen for 9 wt% MWCNT/PLA nanocomposites is probably a result of good filler dispersion. The loadings above 3 wt% of graphene lead to a slightly lower Young’s modulus of the nanocomposites. This Young’s modulus reduction is insignificant and might be related to some negligible inhomogeneous distribution of carbon filler in the polymer, especially at 9 wt% GNP concentration.

![Graph showing Young's modulus vs. carbon nanofiller content for MWCNT/PLA and GNP/PLA composites.](image)

**Figure 9.** Tensile test results presenting Young’s modulus vs. carbon nanofiller content for MWCNT/PLA and GNP/PLA composites.

3.5. SEM Analysis

SEM microscopy has been used to get a detailed characterization of carbon nanotubes in polymer-based nanocomposites [53,54]. In the present work, a series of SEM micrographs applying different magnifications were made to investigate the GPNPs and MWCNTs dispersion state in the composites. Two selected SEM cross-section images of monofiller nanocomposites 9 wt% MWCNT/PLA (Figure 10a) and 6 wt% GNP/PLA (Figure 10b) disclosed a high degree of structure porosity and good uniform insertion of carbon nanofillers within the PLA matrix.
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Figure 9. Tensile test results presenting Young's modulus vs. carbon nanofiller content for MWCNT/PLA and GNP/PLA composites.

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Figure 10. SEM micrographs of 9 wt% MWCNT/PLA (a) and 6 wt% GNP/PLA (b) nanocomposites.

4. Conclusions

Raman spectroscopy appears to be a suitable technique for analysis of the molecular morphology and structure homogeneity regarding PLA-based composites containing graphene or carbon nanotubes. The sensitivity of Raman spectroscopy to highly symmetric covalent bonds makes it capable of catching out even weak changes in structure and uncovers the method as a valuable tool in the characterization of carbon nanomaterials. The I_D/I_G and I_2D/I_G ratios of the nanocomposites are an indication that above 3 wt% carbon filler loading the MWCNT's influence on the compound's chemical structure and properties is more significant.

The effect of multi walled carbon nanotubes on composite crystallinity is noticeable and rises with nanocomposite loading. This fact correlates to the received higher tensile strength, elongation at ultimate strength and Young's modulus values for composites reinforced with carbon nanotubes compared to the neat PLA. The incorporation of graphene in the composite matrix seems to have the opposite influence as the crystalline properties of PLA completely disappear at 9 wt% GNP loading. Carbon nanotubes promoted higher compound crystallinity, which could be a result of their higher degree of functionalization, where carboxyl groups can act as crystallinity centers in the polymer matrix. XRD tests of graphene nanocomposites revealed that the spacing between the platelets in the nanocomposites was slightly affected by the shearing during melt-mixing, resulting in a shift in the graphite (002) peak position. Generally, by increasing the carbon nanotube content, the tensile properties are improved as a result of better filler dispersion in the polymer matrix, confirmed as well by SEM analysis.

Author Contributions: The study was conceived and designed by R.K. and P.C.; T.B. and I.P.-D. performed tensile experiments; V.G. and V.A. were involved in nanocomposites extrusion and samples preparation; T.B., M.C. and C.C. made Raman and XRD investigations; T.B. and R.A. fulfilled SEM analysis; M.S. and E.I. analyzed the data; T.B. wrote the paper.

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