Abstract: In this paper, a water driven soft actuator is introduced. Soft actuators driven by various external stimuli, such as air pressure, temperature, pH, electric field, and light have been reported in the past. Although they are very attractive, they often require hard external devices for driving and the response speeds are often slow. The developed water driven actuator was with sodium polyacrylate wrapped by stretchable meshed nylon. Through some experiments, it was confirmed that swell and shrink phenomena of the developed device occur depending on the fluid flow. The phenomena could be found when adequate quantity of sodium polyacrylate was inside of the nylon. The amount of sodium polyacrylate that is required for the phenomenon was investigated. Through the experiments, it was confirmed that the displacement and the response speed of the swell and shrink were large and fast, respectively, in spite of its simple implementation.

Keywords: soft actuator; water driven actuator; sodium polyacrylate; stretchable meshed nylon

1. Introduction

Soft actuators and soft robots are actively studied due to its safety and flexibility in recent years [1]. There are many studies on soft robots aiming to be used in real environments. Soft robots have useful features that are used in real environments, such as high compatibility and safety with the environment [2,3]. Soft robots can enter a narrow space where a hard robot cannot enter as they have flexible structures and can change its own shape due to their softness [4]. It is also hard to damage even if it receives a strong impact, such as falling unlike hard robots [5]. Soft actuators and soft robots are expected to be used in various situations. There are many approaches to achieve soft actuators.

An approach to achieve soft actuation is to employ air pressure. Pneumatic actuator is a well-known actuator using the mechanical constraints. McKibben actuator is an old example of this approach [6,7]. It is composed of rubber tube and non-stretchable mesh and shrinks about 25%. It is used in various scenes, such as worm-like robot [8], quadruped robot [9], humanoid [10,11], and infant robot [12], due to its safeness. Some soft robots are also driven by jamming and pneumatic actuator [13,14]. Soft actuators driven by water pressure are also reported [15]. The response speeds of these actuators are relatively fast. However, these soft actuators require hard pumps as the external equipment to be controlled and these hard devices prevent the robot from becoming completely soft.

Some soft actuators using chemical reaction are also reported. There are many kinds of soft actuators that swell and shrink with various stimuli from external environments. They are categorized as stimuli-responsive polymers (or composite) and they become increasingly important. They are driven by various stimuli, such as temperature [16–18], pH [19,20], electric field [21], and light [22]. These types of actuators can swell and shrink depending on the external stimuli without using mechanical parts, such as motors, drive shafts, gears, battery, and so on. We can find many mechanically deformable materials that are composed of stimuli-responsive polymers. The survey on stimuli-responsive polymers on actuation shows some examples [23], such as self-folding liquid.
crystal elastomer-based actuators, carbon-based nanomaterials, nafion-based actuators, and so on. It categorized them into liquid crystal elastomer-based actuators, dielectric-elastomer-based actuators and ionic-polymer-based actuators. The developed soft actuator is composed of the particle of sodium polyacrylate and nylon pouch. Although sodium polyacrylate is an ionic-polymer and inside the device, the actuation of the device is due to the mechanical structure of the actuator. The proposed actuator is very simple and has some good points compared to existing actuators. The actuator is a kind of water driven soft actuator, and swells and shrinks depending on the amount of the water flow. In spite of its simple implementation, the response time of swell and shrink is very fast like mechanical approaches. The device is a fully soft actuator with safe and human-friendly materials, unlike some soft actuators with dangerous materials. It is expected that passive scale changeable spiles depending on the water flow and actuators for robots driven by the sea tide and rain are potential applications of the proposed devices. The rests of the paper are organized as follows. In Section 2, the chemical feature of the sodium polyacrylate is briefly explained and the design of the proposed actuator is introduced. The mechanism of the swell and shrink of the proposed actuator is also discussed. In Section 3, some of the experimental results are shown to clarify the response speed, the duration rate and the force of the proposed actuator. Conclusions follow in Section 4.

2. Materials and Methods

2.1. Theoretical Analysis

This section gives the feature of sodium polyacrylate and the mechanism of its high water absorption. Its chemical formula is described, as follows:

\[
\text{CH}_2 \text{CHONa}^+O^- n
\]

The high water absorption of sodium polyacrylate is due to having a hydrophilic carboxyl group. Figure 1 shows the swell mechanism of sodium polyacrylate. As shown in Figure 1, sodium polyacrylate captures numerous water molecules in the network structure when it is immersed in water. It is a superabsorbent polymer. Some experiments were conducted to check its feature. It could be confirmed that it has the ability to absorb more than 100 times its mass in water. Sodium polyacrylate is known as safe human-friendly material and is widely used for various applications, such as disposable diaper, ice pack, lotion, and gardening. Although the absorption ability of the sodium polyacrylate is very high, the swell is basically irreversible. In other words, once the sodium polyacrylate catches the water, it keeps the water well and it does not release the water normally. Although the feature is good for current applications such as disposable diaper and gardening, it is not suitable for actuators to be used repeatedly. To solve the problem, a developed soft actuator was with particles of sodium polyacrylate wrapped by stretchable meshed nylon. Its design is very simple. Figure 2 shows the fundamental design of the proposed actuator. Unlike normal use of sodium polyacrylate, wet sodium polyacrylate was used for the actuator. Hence, the displacement of the proposed device is not due to that from dry sodium polyacrylate to wet sodium polyacrylate. Figure 3 shows the examples of the motion of the developed device. As shown in Figure 3, the device swells and shrinks depending on the water flow. Unlike normal situation, the process is reversible, that is, the reaction occurs cyclically depending on the water flow. It is considered that this phenomenon is due to the physical constraints of nylon. Here, the mechanism of actuation of the proposed actuator is described. Figure 4 shows the response comparison depending on the quantity of sodium polyacrylate. As shown in Figure 4, the swell and shrink response occur only when the quantity...
of sodium polyacrylate is adequate. In this case, the quantity of sodium polyacrylate was 16 g in a 3 cm × 3 cm nylon bag. The phenomena do not occur not only when there is little sodium polyacrylate in the nylon but also when there is an excessive quantity of sodium polyacrylate in the nylon.

Figure 1. Water absorption mechanism of sodium polyacrylate.

Figure 2. A basic design of water driven soft actuator; The sodium polyacrylate is wrapped by the stretchable meshed nylon. If the quantity of the sodium polyacrylate is adequate, the device can swell and shrink depending on the water flow.

Figure 3. Example of the proposed actuator when the water flows to the device and stops.
In this case, the quantity of sodium polyacrilate was 30 g in 3 cm × 3 cm nylon bag (for movies, see Supplementary Information). Empirically, the actuator does not work very well when the nylon is strongly pulled by the sodium polyacrilate. Figure 5 shows the internal structure of the proposed device. As shown in Figure 5, the particles of sodium polyacrylate are fulfilled in the nylon. The quantity of sodium polyacrilate is too large, its effect cannot be ignored. The volume swells stops when all the pressures balances, as follows:

\[ \Delta V = (V_{in} - V_{out}) \Delta t \]

Figure 4. Response comparison depending on the quantity of sodium polyacrilate (for movies, see Supplementary Information).

<table>
<thead>
<tr>
<th>Quantity of sodium polyacrilate</th>
<th>Water is stopped.</th>
<th>Water is poured.</th>
<th>Results</th>
</tr>
</thead>
<tbody>
<tr>
<td>None</td>
<td></td>
<td></td>
<td>No swell and shrink</td>
</tr>
<tr>
<td>Adequate</td>
<td></td>
<td></td>
<td>Swell and shrink</td>
</tr>
<tr>
<td>Excessive</td>
<td></td>
<td></td>
<td>No swell and shrink</td>
</tr>
</tbody>
</table>

Let \( V_{in} \) and \( V_{out} \) be the volume of the incoming water and the outflowing water per unit time, respectively. The volume difference \( \Delta V \) is obtained, as follows:

\[ \Delta V = (V_{in} - V_{out}) \Delta t \]
$V_{out}$ becomes big depending on the swell of the actuator, while $V_{in}$ is constant when the water flow is constant. Let $V_0$ be the initial volume of the proposed device. The device keeps the water when its volume is $V_0$ due to the feature of sodium polyacrylate. Therefore, $V_{out}$ can be described as a linear approximation, as follows:

$$V_{out} = \alpha (V - V_0)$$

where $\alpha$ is a proportionality constant. Hence, the relation between the time and the volume as a linear time-invariant system and the differential equation can be obtained, as follows:

$$\frac{dV}{dt} = (V_{in} - \alpha (V - V_0))$$
As the results, $V$ can be described as follows:

$$V = C_1 e^{-at} + C_2$$

where $C_1$ and $C_2$ are constants of integration. Let $V_{eq}$ be the maximal volume when the device is equilibrium condition. When $t = 0$, the device does not swell. Hence, $V(0) = V_0$. When the device is in equilibrium condition, the volume of the device reaches $V_{eq}$. Hence, $V(\infty) = V_{eq}$. As the results, the following equation can be obtained.

$$V = (V_0 - V_{eq})e^{-at} + V_{eq}$$

Hence, the relation between the time and the volume difference should be as shown in Figure 7.

![Figure 7](image_url)

**Figure 7.** Relation between the time and $V$ modeled by a linear time-invariant system when the actuator swells and shrinks, respectively. (a) Relation between the time and $V$ when the actuator swells; (b) Relation between the time and $V$ when the actuator shrinks.

On the other hand, $V_{out}$ becomes small depending on the shrink of the actuator, while $V_{in}$ is 0 when the water stops. Hence, the differential equation can be obtained, as follows:

$$\frac{dV}{dt} = -\alpha(V - V_0)$$

where $\alpha$ is a proportionality constant. It can be solved by the same logic as the swell case. $V$ can be described, as follows:

$$V = C_3 e^{-at} + C_4$$

where $C_3$ and $C_4$ are constants of integration. When we set the state of the equilibrium condition to $t = 0$, $V(0) = V_{eq}$. After sufficient time, the volume of the device returns to $V_0$. Hence,

$$V = (V_{eq} - V_0)e^{-at} + V_0$$  \hspace{1cm} (1)

The time constant $\tau$ can be set when a linear time-invariant system is considered. When the water flows to the device, the time constant is described, as follows:

$$\tau = (1 - e^{-1})(V_{eq} - V_0)$$  \hspace{1cm} (2)

On the other hand, when the water stops, it is described, as follows:

$$\tau = e^{-1}(V_{eq} - V_0)$$  \hspace{1cm} (3)

Therefore, the relations between the time and the volume are as shown in Figure 7.
2.2. Experimental Setup

Figure 8 shows the parameters measured by the experiment. \( h_{\text{before}} \) and \( h_{\text{after}} \) are defined as the height when the water stops and the height when the water flows, respectively. \( \Delta h \) is defined as the height difference between \( h_{\text{before}} \) and \( h_{\text{after}} \). To investigate the feature of the proposed device, \( h_{\text{before}} \) change and \( h_{\text{after}} \) change, depending on the mass of the sodium polyacrylate, were measured to find the adequate design of the proposed device. The rising time \( t_r \) and the falling time \( t_f \) were also measured respectively to clarify the response speed of the proposed actuator. Three types of nylon pouches were prepared. Their sizes were 10 mm \( \times \) 10 mm, 30 mm \( \times \) 30 mm, and 50 mm \( \times \) 50 mm nylon pouch, respectively. Sodium poly-acrylate was injected into them. The nylon was cut from the ladies stockings made by Dinos Cecile Co., Ltd., Tokyo, Japan. The general Young modulus of the nylon is 2–4 GPa [24]. It was sewn into a rectangle after injecting sodium poly-acrylate. The diameter of the particle of the sodium polyacrylate was from 150 to 710 \( \mu \)m. Swell and shrink of the proposed actuator were observed and recorded using a camera (CASIO Corp. EX-ZR1800, Shibuya-ku, Tokyo, Japan).

![Figure 8: Fundamental parameter of the proposed actuator to be measured in the experiments.](image)

3. Results

3.1. Experimental Results on Displacement and Response Speed of the Soft Actuator

In the experiment, the displacement is measured depending on the quantity of the sodium polyacrylate. The flowing water was set to 15 mL/s. Before the experiment, the actuator was dipped in water for five minutes. Although it is difficult to say that the device reaches equilibrium state of swelling, the swell rate after five minutes becomes much smaller than that when the device was just put in water. Figures 9–11 show the relation between the mass of the sodium polyacrylate in the nylon and the height of the actuator when 1 cm \( \times \) 1 cm, 3 cm \( \times \) 3 cm, and 5 cm \( \times \) 5 cm nylon bags, respectively. The weight of sodium polycrylate represents the weight of wet sodium polycrylate through the paper. In Figure 9, the heights before and after pouring water were equal when the mass of the proposed actuator was 0.1, 1.1 and 1.5 g. As shown in Figures 9–11, a similar tendency could be found in spite of using different size of actuators. The height difference \( \Delta h \) is very small when the mass of the sodium polyacrylate is very small and very large. For example, when the mass is around 10 to 20 g in 3 cm \( \times \) 3 cm, the swell and shrink become large. The displacement rate is around 40% to 50%. The time constant were also measured to check the response speed. The water was poured on the actuator and the movement of the actuator was measured by using image analysis. The time constant was around 0.03 to 0.07 s in both cases. The response speed is very fast when compared to typical soft actuators (for movies, see Supplementary Information).
Large displacement could be obtained.

**Figure 9.** Fundamental parameter of the proposed actuator to be measured in the experiments when 1 cm × 1 cm nylon bag was used.

Large displacement could be obtained.

**Figure 10.** Fundamental parameter of the proposed actuator to be measured in the experiments when 3 cm × 3 cm nylon bag was used.

Large displacement could be obtained.

**Figure 11.** Fundamental parameter of the proposed actuator to be measured in the experiments when 5 cm × 5 cm nylon bag was used.
3.2. Experimental Results on Water Flow and Force of the Soft Actuator

Some experiments were conducted to check the relation between the water flow and the force. A 3 cm × 3 cm nylon bag were prepared and sodium polyacrilate was injected. The quantity of sodium polyacrilate in 3 cm × 3 cm the nylon bag was set to 16 g. The actuator was placed against a wall. A tension gauge was placed against it. In the experiments, the water flow was changed and the force depending the water flow was checked. Figure 12 shows the relation between the water flow and the force. As shown in Figure 12, the force basically increased when the water flow increased.

Demonstration experiments were also conducted to show the potential of the proposed actuator. In this experiment, the actuator was set against a wall and a 100 g object was placed against it. The quantity of sodium polyacrilate was 16 g in 3 cm × 3 cm the nylon bag. Figure 13 shows the demonstration in which the actuator moves the 100 g object. It moves about 5 mm, which corresponds to the displacement of the actuator. To clarify that the work is due to the developed actuator, the results of comparison experiment is also shown. In the comparison experiment, the device was taken out and the water was just poured to the place where the device was set. Although we changed the strength of the water flow, the object did not move, as shown in Figure 14 (for movies, see Supplementary Information).

![Figure 12](image1.png)  
**Figure 12.** Fundamental parameter of the proposed actuator to be measured in the experiments when 3 cm × 3 cm nylon bag was used. The quantity of sodium polyacrilate was set to 16 g.

![Figure 13](image2.png)  
**Figure 13.** Demonstration in which an actuator moves a 100 g object (for movies, see Supplementary Information).
3.3. Experimental Results on Water Flow and Path through the Soft Actuator

Another concept of usage of the proposed device was shown in this section. Figure 15 shows the concept of this application. The supposed application is a kind of scale changeable spile. As shown in Figure 15, the device is set inside the tube in the current scenario. To fix it, the mesh to keep the device will also be set. When the amount of water flow is low, the device does not swell very much and it is expected that the water goes through the tube. On the other hand, when the amount of water flow is high, the device swells and it becomes like a spile in the tube. As the results, it is expected that the water does not go through the tube. Some experiments were conducted to check whether this application is possible. The hold with 3 cm radius hole was set on its top and the hole was covered with mesh. Then, the circular nylon bag with radius 3 cm and with 9 g sodium polyacrilate was set on the hole covered with mesh. The experiments were to check how much the water went into the hold depending on the water flow. Through the experiments, the water hardly entered the hold ($\leq 10 \text{ mL/min}$) when the amount of the water flow is high, while the water entered the hold ($100 \text{ mL/min}$) when the amount of the water flow is low. Figure 16 shows the examples of the experiments. As shown in Figure 16, in both cases, the hole was covered with the device. However, the water went into the hold through the interspace when the amount of the water flow was low, while the water could not go into the hold when the amount of the water flow was high, as the device swelled and the interspace was blocked (for movies, see Supplementary Information). It was also confirmed that the water was hard to pass through the proposed device through the experiment. The results support the possibility that the proposed device can be applied to scale changeable spiles.
The amount of water flow was small.
The device swells and the water was hard to pass through.

Figure 15. Another application of the proposed device as a scale changeable spile.

No water was poured.
The device swells and the water was hard to pass through the proposed device.
Water was poured.
The amount of water flow was large.
The amount of water flow was small.

Figure 16. Another application of the proposed device as a scale changeable spile (for movies, see Supplementary Information).

4. Conclusions

In this paper, a simple water driven soft actuator was introduced. Although the device design is very simple, the displacement is around 40% to 50%. The time constants were within 0.1 s.

The displacement and response speed are large and fast when compared to typical soft actuators. The force of the actuator is measured and a demonstration was shown to clarify that the proposed device can move the object as an actuator. Another scenario of the proposed device as a scale changeable spile was also shown and simple experimental results were given. The constituent material of the proposed actuator is safe and high affinity for humans as it is composed only of the sodium polyacrylate and nylon. The cost required for that actuator is less than 10 cents per an actuator. It is a very inexpensive actuator when compared to other actuators. Through the experiments, the feature and the potential of the actuator could be confirmed. I would like to study more deeply about the applications as scale changeable spiles depending on the water flow. I also would like to develop robots that are driven by the sea tide and rain for future. Theoretical analyses of the proposed actuator should also be done for further studies.

**Funding:** This research received no external funding.

**Conflicts of Interest:** The author declares no conflict of interest.

**References**


20. Fundueanu, G.; Constantin, M.; Bucatariu, S.; Ascenzi, P. pH/thermo-responsive poly(N-isopropylacrylamide-co-maleic acid) hydrogel with a sensor and an actuator for biomedical applications. *Polymer* 2017, 110, 177–186. [CrossRef]


