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Measuring and Modelling Soil Evaporation in an Irrigated Olive Orchard to Improve Water Management

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Abstract: The aim of this study was to estimate soil evaporation (Es) in an intensive olive orchard. Measurements of Es were performed for 19 days using microlysimeters, during summers 2010, 2011 and 2012 in southeast Portugal. In order to relate each area type to radiation transmissivity, ground cover measurements were performed over the years. These data were used to calibrate and validate an empirical model for Es estimation. Measured daily average Es was 0.55 ± 0.14 mm; the model estimated 0.53 ± 0.18 mm for the same days, with a determination coefficient of 0.94. This corresponds to 9% of the reference evapotranspiration, representing well the overall values estimated for the summer, except for days after rain. Regarding the wet area, measured Es for the validation data set was 2.42 L/(m² of wet area), the estimated was 2.49 L/(m² of wet area). Measured average Es in dry area (validation data set) was 0.42 L/(m² of dry area), estimated Es was 0.43 L/(m² of dry area). The large exposed dry area had a significant contribution to evaporation. On average, estimated Es during a typical Mediterranean summer was 10% of reference evapotranspiration, representing 30% of transpiration and 23% of evapotranspiration.

Keywords: lysimeters; evapotranspiration; irrigation; light interception; transmissivity

1. Introduction

In regions where summer water scarcity will not allow intensive agriculture, irrigation is essential to maintain high and constant levels of production. For this reason, there was a significant worldwide expansion of irrigated areas at the end of the 60s, playing a primary role in increasing food production. Later, in the 80s, the expansion of new irrigated areas slowed down due to several factors, including lower performance and higher costs than expected [1]. Therefore, improvement of agricultural water use efficiency is a key issue to alleviate the pressure on water resources of the ever-expanding world population [2]. In areas, where, for climatic reasons, the agricultural sector consumes more than 80% of renewable water resources, a 10% increase in global water use efficiency by the agricultural sector would allow 40% more water for domestic and industrial use [3].

Improving agriculture water use efficiency requests assessing the crop water requirements, allowing optimization of scheduling strategies that, together with the use of more efficient irrigation
techniques, result in more water-conservative agriculture. The evaporation estimation is particularly critical in any crop with a large ground area exposed to radiation and turbulence.

Studies about soil evaporation ($E_s$) suggest that total evaporation from wet soil, in the first phase, is determined primarily by the solar energy reaching the soil surface [4–6] and could, therefore, be reduced by shade [7]. In fact, for a wet soil, $E_s$ is driven and limited by the energy available at the soil surface, at least until cumulative $E_s$ attains the threshold between phase 1 and 2 ($U$, upper limit of cumulative $E_s$ during the first stage, using nomenclature and description in the original publication [5]). After this energy-limited stage, $E_s$ switches to a soil-limited rate (or falling rate stage), usually expressed as an empirical function of time [5]. In this second phase, the soil evaporation rate is determined by soil hydraulic properties, being not completely independent from meteorological variables [4,6,8,9].

Soil evaporation can be measured (ground truth data) by applying water balance methods including lysimeters (e.g. [10–12]), chamber methods and also from micro-meteorological methods if applied in a large continuous surface. These methods are expensive and some are very labor and time consuming [10,13,14]. Modelling is a common approach to overcome these limitations, by measuring soil evaporation over a short period of time and subsequently using the data to calibrate and validate a model to estimate $E_s$ over a larger time frame. There are mechanistic models for which detailed information about system parameters and variables are necessary, for example the Penman-Monteith equation with appropriate conductance of soil surface [15] and its modifications (e.g. [16]) or semi-empirical (or empirical) models [5,8,9]. However, the complexity of the canopy geometry with variable positional shadings along the days and seasons, which overlap with the individual geometry of the wet surfaces, makes it quite difficult to solve. Complex models require input data difficult to obtain in some cases. The semi-empirical models are simpler and consequently of lesser applicability but, after proper calibration and validation, they can provide a robust though only locally valuable estimate, as has been shown in several studies (such as [13,17,18]).

The aim of this study was to create a site-specific model for estimating $E_s$ during three irrigation seasons in an olive orchard in Portugal. To calibrate and validate the model, microlysimeters have been used to carry out in-situ measurements of $E_s$.

This approach allows the user to get $E_s$ along the season and for the partition of evapotranspiration ($ET$) into its components (transpiration, $Tr$ and $E_s$). A locally adjusted $E_s$ model also enables the researchers to obtain $Tr$ as $ET-E_s$, when $ET$ is available, for instance from occasional eddy covariance measurements. These results of $Tr$ can be compared with sap-flow (sap flux density) measured in the stem of the plants which would correspond to approximately $Tr$ at daily scale. Sap-flow outputs can be obtained by several techniques, using an analogy between heat and mass transport, for instance using heat as a marker. Very often (e.g. [19]), sap flow outputs have only relative value, due to the simplified assumptions and technical limitations, so the in-situ “calibration” is highly recommended. This strategy has been used to perform the required corrections to the sap flow outputs in order to get long-term reliable $Tr$ estimates [19]. This operational aim requires daily values of $E_s$ along the season.

2. Materials and Methods

2.1. Site Description

The experimental site was located in the southeast of Portugal, in Alentejo region (38°1.34′ N, 8°10.84′ W), situated at 97 m above sea level. The field was a private olive orchard (*Olea europaea* ‘Arbequina’), established in September 2004 with a spacing of 4.8 × 7 m on a total area of 10 ha inserted in a larger olive orchard area of 434 ha, with lines oriented 330° N.

The local climate is temperate of the Mediterranean type, characterized by mild and wet winters, and very hot and dry summers (Csa—Köppen-Geiger classification). For Beja (nearby main meteorological station), the average annual rainfall is about 580 mm, of which 5% falls in summer (http://www.ipma.pt/pt/oclima/normais.clima/1971-2000/002). The nearest weather station for air temperature, air humidity, incident radiation, wind speed, and rainfall measurements was located
in “Herdade do Outeiro”, about 12 km from the experimental site (www.cotr.pt, SAGRA network). Based on this data, reference evapotranspiration ($ET_0$) was calculated, according to the classical Penman-Monteith equation [15] with grass parameters [20].

The soil was classified as Luvisol [21], type ApBtC, derived from sandy rock with an Ap (0–0.5 m) horizon with loam texture with abundant gravel, a Bt (0.5–1.3 m) horizon with clay texture with few gravel and an horizon C (1.3–2.3 m) with a sandy-loam texture with some gravel. Apparent soil densities of these three horizons were 1.6 g/cm$^3$, 1.4 g/cm$^3$ and 1.8 g/cm$^3$, respectively. A detailed description of the experimental site, soil and field measurements has been given [19], in the context of a larger study.

The orchard was drip irrigated, with the drippers spaced about 0.75 m and located on the tree rows. Irrigation was applied by the farmer generally during night for a few hours, almost on a daily basis (except on early and late season or in case of failure), from late spring to late summer. On average, irrigation depths were 1.3 mm/day, 1.4 mm/day, and 1.7 mm/day in 2010, 2011 and 2012, respectively, with total irrigation volumes of 159 mm, 141 mm and 226 mm in the three irrigation seasons. In 2012, the irrigation volume was higher (about +60% relative to 2011) to account for lower precipitation during the very dry hydrological year (about −46%). The wet area was estimated as 5.7% of the total area (1.91 m$^2$ per tree, tree social area corresponding to 33.6 m$^2$).

### 2.2. Measurement of Soil Evaporation

Daamen et al. [22] developed a protocol for the use of microlysimeters (ML) based on field trials determining the minimum dimensions and the time for which the soil sample is representative of the external soil conditions for different soil water contents. The design and use of ML in this study are based on recommendations of the cited authors and this team experience [23–25].

Evaporation measurements were carried out with 10 MLs, locally built of polyethylene (PE) tubing, with 0.16 m internal diameter and 0.12 m height. Cutting edges have been sharpened to facilitate insertion in the soil. The ML was filled-in by pushing it into the soil up to the full height, every time with a new undisturbed soil monolith taken from a correspondent location. After the complete insertion, the soil around was excavated to insert the bottom (metal plate) and remove the ML. These simple ML were sealed by putting adhesive tape linking the wall and bottom.

However, in order to adequately quantify evaporation from the soil monolith, it is necessary to prevent any loss of weight in the ML that is not caused by evaporation. Consequently, in the case of MLs of wet area, uncontrolled water losses by percolation were avoided by installing an additional PE box at the bottom. This allows the free drainage of the soil monolith, almost as in natural conditions, collecting percolated water in the bottom-box and weighing it together with the ML. The separation between the two parts (monolith and closed drainage chamber) consisted of a fine metal grill allowing drainage. The two parts were linked by adhesive tape sealing the ML.

The ML were cleaned, weighted and inserted into their correspondent location with the undisturbed soil sample (Figure 1a). In order to minimize disturbance and to facilitate recurring MLs removal for weighing during the campaign, additional external PE cylinders were installed in the soil. These outer envelopes remained undisturbed in the soil for the total study period.

At any given measurement time, MLs were removed from the outer envelopes, cleaned, weighed and returned to their respective locations. The soil MLs in the wet area were renewed for every irrigation day, while in dry soil every 2 days, on average. This procedure, normally used on herbaceous row crops [26,27], might cause soil disturbance around the measurement location and could affect evaluation of $Es$. In row crops, this problem is minimized by filling the MLs with soil cores from areas similar to the measurement point and placing them into the fixed outer envelopes. Soil evaporation was gravimetrically measured, using an electronic scale with 0.1 g resolution.

Measurements have been carried out during the summer seasons: 4 days of records in 2010 and 2011, respectively, and 11 days in 2012, for a total of 19 days of measurements.
Depending on multiple factors, $Es$ variability might be high due to local microclimate characteristics, variability in soil water content and soil properties [7]. Thus, the area projected by the crown was expected to be the low irradiation zone during the day, since it remains in shade at noon, the most important period to discriminate between sunny or shaded soil $Es$ rate [7]. In order to discriminate shaded and sunny areas, the olive trees ground cover (GC), representing the projected canopy area on the ground divided by total area of each plant (social area), was measured (next section, Measurement of Radiation Transmissivity and Ground Cover).

The time schedule of $Es$ measurements was half hourly in 2010 and 2011, every 2 hours for 5 days in 2012 and daily (from sunrise to sunset) for all other remaining days.

There were six drippers between two adjacent trees in a row, where each dripper created a wet area with a diameter of $0.6 \pm 0.06$ m. We deployed 10 MLs between two trees (Figure 1b): one ML was installed in each wet area, and four MLs in dry soil, placed at the external part of the row. During irrigation, the dripping line was left in the center of the row to keep the soil around the measurement point representative of the wet area. After irrigation, when MLs were positioned, the dripping line was displaced beside the MLs to avoid random input of water in the MLs and to facilitate the operations. The area in the orchard where ML could be practically installed was only on the tree rows or close to it, because of high soil compaction between the rows, caused by heavy agricultural machinery traffic.

Figure 1. (a) Microlysimeter ready to be inserted in the external cylinder, where it remains until the next weighting; (b) Microlysimeter positions (numbers refer to Figure 2; dripper tube not centered during measurement time).

Figure 2. Scheme of microlysimeters position in a tree row with the shade of two contiguous trees: wet shaded area (A, ML 1, 2, 5, and 6), wet sunny area (B, ML 3 and 4), dry shaded area (C, ML 7 and 8), dry sunny area (D, ML 9 and 10). Dashed circles are wet zones (diameter ca. 0.6 m). Dotted grey bands are the inter-row spaces. Cornered stars are the trunks of the trees.
Each tree social area was split into four areas of the following types: sunny wet, shadow wet, sunny dry, and shadow dry. Four MLs in wet shaded area (A), two in wet sunny (B), two in dry shaded (C) and two in dry sunny area (D) were used (Figures 1b and 2). Shadow wet, sunny wet, shadow dry, and sunny dry area were about, 3.6%, 2.1%, 17.7%, and 76.6% of the total surface, respectively (areas A, B, C, and D, in Figure 2).

2.3. Measurement of Radiation Transmissivity and Ground Cover

Over the course of $E_s$ measurements, daily photosynthetically active radiation (PAR) curves aside the MLs were measured with PAR sensors (Skye instruments Ltd, Llandrindod Wells, UK), with data being recorded by a data-logger (model CR23X, Campbell Scientific, Logan, Utah, USA). These curves were used to calculate PAR transmissivity ($T_{PAR}$), which is defined as the ratio between a reference PAR curve ($I_o$, recorded in a 100 % $T_{PAR}$ position) and the PAR curve of each ML’s position ($I_s$).

The overhead photograph technique [28] was used to measure GC. At our experimental site, pictures were taken from above the trees to determine the crown projected area (as in [29]), using a camera (Model E450 with Zuiko Digital lens 14–42 mm; 1:3.5–5.6, Olympus, Tokyo, Japan) mounted on a 7.5-m-high stick. Squared metal boards with known areas were used as reference objects. To measure the projected area, photos were processed with an image editing software (ImageJ, https://imagej.net/) that recognized crown perimeter. An increase of apparent size emerges by taking images from a fixed height during the growing season or measuring object at different distances, which can lead to an overestimation of GC. A method was established to calculate the error of apparent size in lettuce growth [30], using the distance formula to compare object with different heights and claiming that a decrease of 1% in distance results in a 2% error, while a change in 10% would result in a 23% error.

2.4. Model Description and Validation

The two-stage $E_s$ theory [5] was used, considering wet area in the first stage (energy-limiting stage) and dry area in second stage (falling rate stage). To simulate $E_s$ in a wet area, two models were tested. The first uses the equation presented by Bonachela et al. [31]:

$$E_{s1} = \frac{\Delta}{(\Delta + \gamma)} R_n a + \frac{\gamma}{(\Delta + \gamma)} VPD \times 2.7 \times (1 + \frac{u_2}{100}),$$  

where $E_{s1}$ is soil evaporation during the energy-limiting stage (mm day$^{-1}$), $\Delta$ is the slope of the vapor pressure curve (kPa °C$^{-1}$), $\gamma$ is psychometric constant (kPa °C$^{-1}$), $R_n$ is net radiation (mm day$^{-1}$), $a$ is the PAR transmissivity (calculated as below crown PAR radiation divided by the above crown PAR radiation), $VPD$ is the vapor pressure deficit (kPa), and $u_2$ is wind speed at 2 m height (km day$^{-1}$). Equation (1) is identical to the Penman $ET_0$ equation (concerning wind function), except for the parameter $a$ in the radiation term of the equation and for not using the adjustment factor of Doorenbos and Pruitt [32]. However, given the shape of the wet area and its arrangement in a long row, the wind function in Equation (1) (2.7 (1 + $u_2$/100) was modified, using the one presented for elongated water bodies [33]:

$$f(u_2) = (2.33 + 1.65 u_2) L^{-0.1},$$  

where $u_2$ is wind speed at 2 m height (m s$^{-1}$), and $L$ is the average width of the water surface. Therefore, combining Equations (1) and (2), the modified equation is:

$$E_{s1} = \frac{\Delta}{(\Delta + \gamma)} R_n a + \frac{\gamma}{(\Delta + \gamma)} VPD \times (2.33 + 1.65u_2) L^{-0.1}. $$

The second model obtains $E_s$ from a wet surface under a canopy as follows [9]:

$$E_{s1} = ET_0 K_e \left(1 - \frac{R_s}{100}\right),$$
where $K_r$ is a coefficient calculated as a function of $ET_0$ rate and wetting frequency (time from last rainfall or irrigation, similarly to Equation (5)) and $(1-R_i/100)$ is the fraction of daily radiation ($R_i$) reaching the soil, here assumed equal to PAR transmissivity of Equations (1) and (3).

To estimate $Es$ in a dry area, the falling rate stage equation established by Ritchie [5] was used:

$$Es_2 = C (t^{0.5} - (t - 1)^{0.5}),$$

where $Es_2$ is daily soil evaporation during the falling rate stage (mm day$^{-1}$), $t$ is time (days) elapsed from the day following rain, and $C$ is a soil parameter (mm day$^{-0.5}$).

The model performance was verified by testing the linear correlation (coefficient of determination, $r^2$), the mean absolute error (MAE) between measured and estimated values, and relative coefficient of residual mass (CRM).

As described in Section 3.4 (Model Calibration and Validation), the results analysis showed that another modification in Equation (3) would be still necessary, obtaining Equation (6).

### 3. Results and Discussion

#### 3.1. Soil Evaporation and Its Relationship with PAR Transmissivity

Partial tree coverage of the under-tree area resulted in high spatial variability of irradiance at the soil surface (example in Figure 3). When comparing the different patterns observed for $TPAR$ with 2-hourly $Es$ values for a high ($ML4, ML10$) and low irradiance location ($ML1, ML7$) beneath the olive crown in wet and dry areas (Figures 3a and 3b, respectively), $Es$ follows the course of the $TPAR$ curve over the day. It shows its maximum between midday and 4 p.m. (legal time = solar time + 1:45), the period with the highest atmospheric demand. During this period, the largest difference between $Es$ rates of sunny and shaded areas occurred, while, at the beginning and end of the day, $Es$ values were similar (Figure 3). Shaded areas had lower values for maximum total daily $Es$ than sunny areas, confirming that GC provides a good indication for the purpose of discriminating high and low $Es$ areas.

![Figure 3](image_url)

**Figure 3.** Daily $Es$ curve (circle for wet area, triangles for dry area; empty symbols for sunny area, filled symbols for shaded area) and $TPAR$ curve (dashed lines) for two wet (a) and two dry (b) MLs, with high irradiance ($TPAR\_ML4$ and $TPAR\_ML10$) and low irradiance ($TPAR\_ML1$ and $TPAR\_ML7$). Note that there was condensation (represented in the graph as negative $Es$) starting in late afternoon for dry MLs ($ML7$ and $ML10$). Legal time is shown.

During the energy-limiting stage (wet area), the $Es$ ratio depends strongly on the incoming solar radiation curve, with an apparent slight delay in time (Figure 3a). However, even $Es$ in the dry area did not seem to be completely independent from solar radiation (Figure 3b), showing a decrease in $Es$ with less irradiation and an increase of $Es$ with greater irradiation reaching the soil. This response to incoming energy was not as strong as in the first stage of evaporation, but a slight connection between irradiation and $Es$ ratio is observable. The explanation can rely on the relationship between solar...
radiation and vapor pressure deficit daily courses, as well as, on increasing soil surface temperature impacting sub-surface evaporation; the water vapor flux originated below the surface, becoming the dominant source for this second stage, as suggested by other researchers [34,35].

Wet pairs MLs positioned in the mirror (1 and 6, 2 and 5, 3 and 4) had very similar behavior with respect to daily evaporation, suggesting that the division of the areas well reflected $E_s$ variability.

A lower irradiance zone was observed within a radius of approximately 0.85 m from the trunk, with average $P_{AR} = 14\%$, while a medium irradiance zone was detected down the external part of the crown (from the internal circle to the higher transmissivity zone), with average $P_{AR} = 34\%$. Thus, the weighted average $P_{PAR}$ for the overall shaded area was 28%. The higher transmissivity zone between two trees in row, outside of the canopy projection on the ground, had an average $P_{PAR}$ of 67%. Calculated average $P_{PAR}$ for wet (A+B) and dry (C+D) areas were 43.3% and 56.4%, respectively.

On the inter-row dry zone, mainly exposed to the sun, no MLs were installed due to the impenetrability of the hard soil. Transmissivity in this area was expected to be higher compared to the sunny area within (ML 3 and 4) and closer (ML 9 and 10) to the tree rows. However, there were no differences in $E_s$ between area C (shaded) and D (sunny), although area D had a double $P_{PAR}$. MLs with high variability of $P_{PAR}$ in dry areas had a difference in $E_s$ in the order of tenths of a millimeter. On average, the difference between $E_s$ from shaded and sunny dry areas was 6%, based on a very low value. Therefore, we considered differences in $E_s$ fluxes between dry soil close to the row (D) and dry soil inter-row to be negligible, justifying that the results from observations for area D were extended to the entire area between the rows.

Finally, it should be stressed that night condensation (dew) was observed in C and D areas (represented in Figure 3b as negative $E_s$) starting at the end of the afternoon. Consequently, three measurements of night condensation were performed, weighing the MLs at late afternoons and early mornings before the renewal of dry MLs, resulting in an average value of 0.15 ± 0.06 mm and 0.25 ± 0.08 mm, for area C and D, respectively. Agam and Berliner [36], also cited by Shimojima et al. [37], observed that the amount of condensed water in the Negev desert was in the range 0.2–0.3 mm/night, and thus, the same range was observed here.

3.2. Ground Cover Measurements

In 2010, GC was 0.20 (average tree projected area = 5.7 m² [38]), while the GC average value in 2012 (14 August) was 0.30 (average tree projected area = 8.4 m²), resulting in a growth of 48% in 2 years. Pruning between 2012 and 2013 was particularly intense. New GC measurements were carried out in 2013 (5 July), being 0.22 (average tree projected area = 6.20 m²), showing a decrease of 26% from 2012 to 2013.

3.3. Average Soil Evaporation from Measurements

The averaged $E_s$ for the areas A, B, C, and D is presented in Figure 4a (A, B, C, and D zones: 3.6%, 2.1%, 17.7%, and 76.6% of total area). The average daily $E_s$ for wet and dry areas was respectively 2.41 ± 0.73 L/(m² of wet area) and 0.44 ± 0.12 L/(m² of dry area), in the following reported as mm (on wet or dry area basis). Weighted average $E_s$ of all areas was 0.54 ± 0.14 mm/day.

For the dry area, the average $E_s/ET_0$ was 0.07 ± 0.03. To highlight the difference between $E_s$ values of the wet area during irrigation day (day1) and day after (day2), Wallace and Holwill [12] suggested using average daily $E_s/ET_0$ as an indicator phase swift. Average $E_s/ET_0$ of wet area on day 1 was 0.49 ± 0.10 (i.e., 0.028 on total area basis) and it decreased in day 2 to 0.28 ± 0.06 (i.e., 0.016 on total area basis). These values correspond to 0.11 and 0.08 respectively, if $E_s$ of the total area is considered. A test carried out, 3 days after irrigation, showed very low differences in $E_s$ between MLs, with average $E_s/ET_0$ of 0.21 ± 0.01. Figure 4b shows the average daily $E_s$ value for dry and wet areas, divided into $E_s$ for irrigation day and the day after, for wet areas. The maximum evaporation rate was in the wet area for irrigation day, with clear differences between shaded and sunny wet areas. The subsequent
day, $Es$ decreased reaching similar values for both sunny and shaded wet areas. Evaporation flux of the shaded wet area was 22% and 16% lower than the sunny wet area in day1 and day2, respectively.

![Figure 4. Daily ET$_0$ (mm/day) and measured daily $Es$ (mm) for the wet area (A$_{d1}$ and B$_{d1}$, d1 is the day of the irrigation event; A$_{d2}$ and B$_{d2}$, d2 is the second day after the irrigation event) and dry area (C and D). (a) Daily average $Es$ for the areas A, B, C, and D (all days averaged) as well as average $Es$ for the irrigation day (day1) and for the following day (day2) for wet areas (mm/day) (b). Note that missing data from the wet or dry area were excluded due to poor preparation of the MLs.](image)

A direct relationship between $T_{PAR}$ and $Es$ of wet areas over time was found (Figure 5a). The difference between $Es$ in wet area positions decreased, being more independent from $T_{PAR}$, for the day after irrigation. A good relationship between $ET_0$ and $Es$ was found, for both wet and dry areas (Figure 5b), suggesting a dependence of $Es$ during falling rate stage on atmospheric demand, as already stressed.

![Figure 5. Relationship between daily $Es$ for the MLs positions in the wet area (irrigation days: Wet_day1; subsequent day: Wet_day2) and dry area (Dry), and (a) daily $T_{PAR}$ (missing ML6) and (b) daily $ET_0$.](image)

### 3.4. Model Calibration and Validation

Wet area: In order to check the validity of any necessary adjustments, the dataset was split into two samples, in order to have one dataset for calibration and another dataset for validation of the model. For both calibration and validation of the model, nine points were used for wet and dry areas separately (Figure 6a,b), and eight points for averaged $Es$ (Figure 6c).
When comparing the results of the aerodynamic term in Equations (1) and (3) with \( Es \) was registered and wind speed, which was measured at 2 meters height in open field above grass (standard conditions for water (irrigation or rain), the absence of those (Soil Evaporation from Measurements), no clear-cut transition between phase 1 and 2 of evaporation exponent (obtaining Equation (6)). This was possible because, as mentioned in Section 3.3, (Average equation, a time-dependence function (time since last irrigation, \( t \), in the case of the wet soil was strongly associated with the time elapsed since the last wetting) parameters was overcome by adding, in the original Ritchie model [5], an overestimation (about 85%, MAE about 46%) was observed, as expected. However, Equation (3) overestimated \( Es \) by about 70% in day 1 and about 200% on day 2, with a determination coefficient of 0.11 (Figure 6a, Table 1). A reasonable estimation was obtained with Equation (4), but with a low regression coefficient (Figure 6a, Table 1). When comparing the results of the aerodynamic term in the Equations (1) and (3) with \( Es \) measurements, an overestimation of 29% and 19%, respectively, was found. One main influencing factor might be the wind speed, which was measured at 2 meters height in open field above grass (standard conditions for meteorological data) not reflecting the wind velocity close to the ground in this rough, highly anisotropic canopy with variable degrees of turbulence below the top of the canopy. To correct the aerodynamic term in Equation (3), a “best fit” approach calibration coefficient named “\( b \)” was introduced (Equation (6)).

\[
Es_1 = \left[ \frac{\Delta}{(\Delta + \gamma)} \right] Rn_a + b[y/(\Delta + \gamma)] \quad \text{DPV} (2.33 + 1.65u_2) L^{-0.1} \left[ (0.67 - (t - 1)^{0.67}) \right].
\]  

Another adjustment was proved necessary. The original Ritchie model [5] could not be applied as a complete soil desiccation cycle was not performed. It was impracticable to determine both values for the parameters of this soil (\( U \) and \( C \)) in the equation of the energy-limiting stage proposed by Ritchie [5]. As \( Es \) in wet soils is strongly associated with the time elapsed since the last wetting (irrigation or rain), the absence of those (\( U \) and \( C \)) parameters was overcome by adding, in the original equation, a time-dependence function (time since last irrigation, \( t \), as in Equation (5)) with a best-fit exponent (obtaining Equation (6)). This was possible because, as mentioned in Section 3.3, (Average Soil Evaporation from Measurements), no clear-cut transition between phase 1 and 2 of evaporation was registered and \( Es/ET_0 \) ratio for wet soil was less than one on irrigation days, decreasing the day after irrigation, suggesting that generally, the irrigation depths (amount of water given per irrigation application) were not enough to bring the bulk soil to field capacity. Most likely the soil already had

<table>
<thead>
<tr>
<th>Evaluation Parameters</th>
<th>Equation (6), Wet ((a = 0.43; b = 0.35))</th>
<th>Equation (4), Wet ((a = 0.43))</th>
<th>Equation (3), Wet ((a = 0.43))</th>
<th>Equation (6), Dry ((a = 0.2; b = 0.6))</th>
<th>Equation (4), Dry ((a = 0.2; b = 0.6))</th>
<th>Equation (5), Dry ((C = 7.5 \text{ mm day}^{-0.5}))</th>
<th>Equation (6), Avg ((a = 0.2; b = 0.6))</th>
<th>Equation (4), Avg ((a = 0.2; b = 0.6))</th>
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<tbody>
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<td>( r^2 )</td>
<td>0.95 ***</td>
<td>0.15**</td>
<td>0.11 **</td>
<td>0.86 ***</td>
<td>0.75 **</td>
<td>0.23 *</td>
<td>0.94 ***</td>
<td>0.78 ***</td>
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<td>Slope</td>
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<td>2.2</td>
<td>0.6</td>
<td>96.1</td>
<td>5.5</td>
<td>2.2</td>
<td>15.2</td>
<td>5.9</td>
<td>2.2</td>
</tr>
<tr>
<td>MAE (mm)</td>
<td>0.15 (6%)</td>
<td>0.4 (17%)</td>
<td>2.12 (86%)</td>
<td>0.05 (12%)</td>
<td>0.07</td>
<td>0.08 (19%)</td>
<td>0.05 (10%)</td>
<td>0.06 (13%)</td>
</tr>
</tbody>
</table>

*Figure 6. Measured vs. estimated values of Es (mm) for wet (a), dry (b) and total area (c), in each case with the parameters shown in Table 1, as before.*

Using the original equation (Equation (1), \( a = T_{PAR} = 0.43 \)), an overestimation (about 85%, MAE about 46%) was observed, as expected. However, Equation (3) overestimated \( Es \) by about 70% in day 1 and about 200% on day 2, with a determination coefficient of 0.11 (Figure 6a, Table 1). A reasonable estimation was obtained with Equation (4), but with a low regression coefficient (Figure 6a, Table 1). When comparing the results of the aerodynamic term in the Equations (1) and (3) with \( Es \) measurements, an overestimation of 29% and 19%, respectively, was found. One main influencing factor might be the wind speed, which was measured at 2 meters height in open field above grass (standard conditions for meteorological data) not reflecting the wind velocity close to the ground in this rough, highly anisotropic canopy with variable degrees of turbulence below the top of the canopy. To correct the aerodynamic term in Equation (3), a “best fit” approach calibration coefficient named “\( b \)” was introduced (Equation (6)).

\[
Es_1 = \left[ \frac{\Delta}{(\Delta + \gamma)} \right] Rn_a + b[y/(\Delta + \gamma)] \quad \text{DPV} (2.33 + 1.65u_2) L^{-0.1} \left[ (0.67 - (t - 1)^{0.67}) \right].
\]  

Another adjustment was proved necessary. The original Ritchie model [5] could not be applied as a complete soil desiccation cycle was not performed. It was impracticable to determine both values for the parameters of this soil (\( U \) and \( C \)) in the equation of the energy-limiting stage proposed by Ritchie [5]. As \( Es \) in wet soils is strongly associated with the time elapsed since the last wetting (irrigation or rain), the absence of those (\( U \) and \( C \)) parameters was overcome by adding, in the original equation, a time-dependence function (time since last irrigation, \( t \), as in Equation (5)) with a best-fit exponent (obtaining Equation (6)). This was possible because, as mentioned in Section 3.3, (Average Soil Evaporation from Measurements), no clear-cut transition between phase 1 and 2 of evaporation was registered and \( Es/ET_0 \) ratio for wet soil was less than one on irrigation days, decreasing the day after irrigation, suggesting that generally, the irrigation depths (amount of water given per irrigation application) were not enough to bring the bulk soil to field capacity. Most likely the soil already had

<table>
<thead>
<tr>
<th>Parameters</th>
<th>Equation (6), Wet ((a = 0.43; b = 0.35))</th>
<th>Equation (4), Wet ((a = 0.43))</th>
<th>Equation (3), Wet ((a = 0.43))</th>
<th>Equation (6), Dry ((a = 0.2; b = 0.6))</th>
<th>Equation (4), Dry ((a = 0.2; b = 0.6))</th>
<th>Equation (5), Dry ((C = 7.5 \text{ mm day}^{-0.5}))</th>
<th>Equation (6), Avg ((a = 0.2; b = 0.6))</th>
<th>Equation (4), Avg ((a = 0.2; b = 0.6))</th>
</tr>
</thead>
<tbody>
<tr>
<td>( r^2 )</td>
<td>0.95 ***</td>
<td>0.15**</td>
<td>0.11 **</td>
<td>0.86 ***</td>
<td>0.75 **</td>
<td>0.23 *</td>
<td>0.94 ***</td>
<td>0.78 ***</td>
</tr>
<tr>
<td>Slope</td>
<td>1.03</td>
<td>0.92</td>
<td>1.8</td>
<td>1.04</td>
<td>1.04</td>
<td>1.03</td>
<td>1.07</td>
<td>1.04</td>
</tr>
<tr>
<td>CRM (%)</td>
<td>2.2</td>
<td>0.6</td>
<td>96.1</td>
<td>5.5</td>
<td>2.2</td>
<td>15.2</td>
<td>5.9</td>
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<td>0.05 (10%)</td>
<td>0.06 (13%)</td>
</tr>
</tbody>
</table>
left phase one and continued to be in the transition phase [5,39]. Díaz-Espejo et al. [40] also concluded that after the first day, $E_s$ process left phase one, observing a six-fold increase in soil surface resistance between the first and second day.

Considering all these modifications (in summary, Equation (6) results from Equation (3) with $a = T_{PAR} = 0.43$ modified with factor $b = 0.35$ and a last term similar to Equation (5)), Equations (4) to (6) were compared for the different situations (wet soil, dry soil, and average), with their specific parameters (Figure 6a, Table 1). In the case of the wet area, the best results were achieved with Equation (6).

Dry area: For Equation (5), the best results were achieved using a best fit $C$ parameter of 7.5 mm day$^{-0.5}$ (Table 1). Notwithstanding, considering the relationship between dry soil $E_s$ and $ET_0$, Equations (4) and (6) were also used to estimate $E_s$ in dry area, with better results than Equation (5) (Figure 6b, Table 1). However, in this case, the best results with Equation (6) were achieved not using $a = 0.56$, that was the average $T_{PAR}$ of dry area, but with factors $a = 0.2$ and $b = 0.6$.

This result suggests that, when $E_s$ was limited by soil hydraulic properties, the aerodynamic term of Equation (6) had a greater influence in determining soil evaporation rates but incident radiation still played a role in driving dry soil evaporation. If analyzing separately the relationship between each term and $E_s$, the following values were observed for $r^2$: 0.93 and 0.84 for the first (energetic) and second (aerodynamic) terms of Equation (6), in the case of the wet area, and 0.63 and 0.85 in the case of the dry area.

Total area: $E_s$ for the total area was estimated using the weighted $E_s$ for wet and dry soil calculated with Equations (4) and (6) (Figure 6c, Table 1) with the best results for Equation (6), as expected. For this total $E_s$ estimated with Equation (6), the respective parameters for wet and dry areas (Table 1) were used.

A sensitivity analysis was made for the impact of changing values of $a$ and $b$ parameters on $E_s$ using Equation (6). A 100% change on $a$ and $b$ impacts $E_s$ in 68.5% and 31.5% of its value, respectively, for $a$ and $b$, in the case of the wet area. For the dry area, the corresponding values are 36.7% and 63.6%, respectively, for $a$ and $b$.

In summary (Table 1), to estimate the $E_s$ of the wet area, a determination coefficient of 0.95 and MAE = 0.15 mm (about 6% relative error) was found in this study. For the dry area, a lower $r^2$ (0.86) and a higher relative error (12%) was found. For the total area, the determination coefficient was 0.94 with a MAE of 0.05 mm (about 10% relative error). In the literature, also in olive orchards, using Equation (1), other researchers [31,41] reported a MAE of 0.30 mm, with $r^2$ of 0.98 for wet areas, and 0.85 for the total area, with higher errors.

3.5. Model Application at Seasonal Scale

Equation (6) was used to calculate $E_s$ for the entire irrigation period when precipitation events were not frequent (Figure 7). In case of rain, when the entire soil surface was wet, $E_s$ was calculated using only the wet area equation (Equation (6), 100% of $E_s$ from wet area). When cumulated $E_s$ reached the cumulated value of the precipitation, total evaporation was calculated as the weighted average of wet and dry areas (5.7% wet area, 94.3% dry area on average for the 3 years).

Analyzing the results within these 3 years of model application (from 15 July to 15 September for the years 2010, 2011 and 2012), daily average was 0.54 mm, 0.84 mm and 0.59 mm, respectively (Figure 7a).

The cumulated $ET_0$ for the month of August for the three years was about 176 mm, 155 mm and 173 mm, respectively; average $E_s/ET_0$ was 0.10, 0.17 and 0.10, respectively (Figure 7b). The higher $E_s/ET_0$, in August 2011, was due to a lower $ET_0$ and higher water availability in the soil for the entire orchard. This can be attributed to higher spring precipitation, as well as several cloudy days and unusual precipitations in August.
Estimated $E_s$ was related to $Tr$: $Es/Tr$ ranged between ca. 0.4 and 0.2 (0.3 on average) during a typical summer such as 2010 with a progressive decrease along the summer, in spite of the permanent dry appearance of the soil surface during the whole of this period and the constant wet area, reflecting the dependence on meteorological conditions, affecting $Tr$ with a different dynamic due to phenology. During 2011, higher estimated $Es/Tr$ was obtained, due to occasional precipitation while, during 2012, the higher values can be explained by an exceptional decrease in transpiration by the end of summer [19] due to severe water stress.

Estimated $E_s$ was also related to total $ET$: $Es/ET$ ranged between ca. 0.30 and 0.15 (0.23 on average) during summer 2010, with the same dynamics as above, for the other years (Figure 7b).

In a peach orchard under the same climate, also drip irrigated and with a slightly higher ground cover of 0.3 (sandy soil, daily irrigation with wetted area fraction of 0.06), Conceição et al. [42] measured $E_s$ from 0.2 mm/day to 0.6 mm/day, $Es/ET_0$ being between 0.05 and 0.12, thus in the same range observed here.

For a super-intensive olive orchard (‘Arbequina’, planted in 2006, spaced 1.35 × 3.75 m, ground cover of 0.35, same climate), Paço et al. [43] measured $E_s$ (8 days during 2011 and 2012). Based on these data, they modeled $E_s$ (implementation of Richie model [5]) considering that, from February to early August (2012), 30% of the soil was covered by mulch resulting from heavy defoliation (frost in February 2012). For 5 months interval, from middle June to late summer, except for rainy days, $E_s$ was
about 1 mm/day, corresponding to ca. 30% of ET, slightly above the values observed here, as expected (in our study distance between dripper lines is double, so wet area could be much less).

In another olive orchard (Cordoba, Spain, ground cover of 40%, double that in the present study for the typical year of 2010), Villalobos et al. [44] measured ET and Es (eddy covariance method, day of the year 171, 172 and 173) when soil surface was dry (although the olive orchard was irrigated) and they concluded that average Es was 0.74 mm/day (for ET of 3.12 mm/day), so Es/ET would be on average 24%, in the range estimated in the present study (0.3 to 0.15, 0.23 on average).

Even though the wetted area by drippers was only 5.7% of the total orchard, the model indicates that about 29% of the evaporated water came from the wetted area in 2010 and 2012, and 19% in 2011 (rain). During a typical dry summer, 71% of Es comes from the “dry” area, which is quite a high fraction. Considering the large exposed area, which is apparently extremely dry, and the turbulence generated around the wet area, with the consequent clothesline effect, it could be expected to observe a higher percentage of total evaporation coming from the wet area.

Part of the water evaporated in the exposed dry area could be available through night condensation (as measured in few days) and also eventually, from deeper layers (vapour transfer from below surface), even under severe dryness, which is typically not considered in evaporation modeling of very dry soils but was noticed by others [39,41] as mentioned in Section 3.1 (Soil Evaporation and its Relationship with PAR Transmissivity).

4. Conclusions

In irrigation management, Es is often seen as “water loss” to the atmosphere, as it cannot directly be used from the crop and users aim to reduce this component by good practices such as localized irrigation. Thus, a correct estimation of Es is necessary for good irrigation practices. Besides, quantifying Es brings the possibility to check validity of the widely disseminated sap flow techniques when compared to micrometeorological techniques that measure total ET, one of the practical aims of this general study.

A total of 19 days of measurements with ML were used to calibrate and validate an empirical model for local Es estimations. The average daily measured Es for wet and dry areas was respectively 2.41 ± 0.73 L/(m² of wet area) and 0.44 ± 0.12 L/(m² of dry area). Weighted average Es for all areas was 0.54 ± 0.14 mm/day.

Best results for Es estimation were achieved with Equation (6) (Table 1), with different calibration factors for dry and wet areas (wet area: $a = 0.43$ and $b = 0.35$; dry area: $a = 0.2$ and $b = 0.6$). Indeed, we found that the radiation term had higher $r^2$ than the aerodynamic term when soil was wetted, while the opposite was found in dry soil. The model overestimated by 6%, with a relative error of 10% and $r^2$ of 0.94.

For the 3 years of model application (July to September, 2010, 2011 and 2012) daily average Es was 0.54 mm, 0.84 mm and 0.59 mm, respectively. During a typical summer such as 2010, Es/Tr ranged between ca. 0.4 and 0.2 (0.3 on average), Es/ET ranged between ca. 0.3 and 0.15 and average Es/ET$_0$ was quite stable around 0.10 (2010).

This study showed that the use of an empirical model for Es estimation provided a robust, locally evaluable estimate, which is useful for evapotranspiration partitioning into its components of evaporation and transpiration with the aim of improved farm water management. Furthermore, the results indicated that a large exposed dry area (77%) had a contribution to evaporation above expectations, which is most likely due to the water available from night condensation and more internal layers. Apart from Es quantification and the adsorption effect, once more it could be confirmed that the complexity of the canopy geometry with variable positional shadings along the days and seasons, overlapping with the individual geometry of the wet surfaces and variable turbulence, makes it very difficult to generalize models for evaporation below crowns.
**Author Contributions:** Conceptualization, methodology, formal analysis, interpretation, original manuscript preparation: L.T.; coordination, conceptualization, data curation, methodology, interpretation: M.I.F.; collaboration in experimental methodology: N.C.; measurements: L.T., N.C., M.H.; text, review and editing: L.T., N.C., M.H, M.I.F.

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