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Pareto Optimal Reconfiguration of Power Distribution Systems Using a Genetic Algorithm Based on NSGA-II

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Abstract: Reconfiguration, by exchanging the functional links between the elements of the system, represents one of the most important measures which can improve the operational performance of a distribution system. The authors propose an original method, aiming at achieving such optimization through the reconfiguration of distribution systems taking into account various criteria in a flexible and robust approach. The novelty of the method consists in: the criteria for optimization are evaluated on active power distribution systems (containing distributed generators connected directly to the main distribution system and microgrids operated in grid-connected mode); the original formulation (Pareto optimality) of the optimization problem and an original genetic algorithm (based on NSGA-II) to solve the problem in a non-prohibitive execution time. The comparative tests performed on test systems have demonstrated the accuracy and promptness of the proposed algorithm.

Keywords: power distribution systems; reconfiguration; genetic algorithms; multi-objective optimization; pareto optimality

1. Introduction

The most important measures which can improve the performance in the operation of a distribution system are: (i) *reconfiguration of the system*, exchanging the functional links between its elements (system/network/feeder reconfiguration problem); (ii) *variation and control of the reactive power flow* through the system (optimal reactive power dispatch problem), using bank capacitors, power generators, etc.; (iii) *variation and control of the voltage* by using on-load tap-changers for power transformers (by using automatic voltage regulators); and (iv) *changing the operating scheme of the parallel connected power transformers, etc.* This paper focuses on optimization through the reconfiguration of power distribution systems.

The reconfiguration problem is one of the multi-criteria optimization types, where the solution is chosen after the evaluation of some indices (e.g., active power losses, reliability indices, branch load limits, voltage drop limits, etc.), which represent multiple purposes. These criteria can be grouped in two different categories: (i) *objective functions*: criteria that must be minimized; and (ii) *constraints* (restrictions): criteria that must be included within some bounds. On the other hand, the criteria are incompatible from the point of view of measurement units and are often conflicting. Moreover, some criteria can be (or it is important for them to be) modeled, at the same time as objectives and constraints. For instance, the active power losses must be minimized but we can simultaneously impose a maximal acceptable value (constraint). Thus, in order to solve the problem, first of all, *a proper model* has to be chosen. The problem of optimization through the reconfiguration of a power distribution system, in terms of its definition, is a historical *single objective problem with constraints*. Since 1975, when Merlin and Back [1] introduced the idea of distribution system reconfiguration for active power loss reduction, until nowadays, a lot of researchers have proposed diverse methods and algorithms to solve the reconfiguration problem *as a single objective problem*. The most frequently used one is *the main criterion method (ϵ -constraint)* where the problem is defined in the following conditions: a main criterion is chosen, concomitantly indicating acceptable values for the other criteria. Usually, active power losses are adopted as the main criterion [1–22]. This approach has a major weakness because there is more than one index that must be taken into account in the optimization process and, without any prior information about the different criteria, choosing the acceptable value can be problematic. Additionally, this approach alters the essence of the original technical problem. On the other hand, some authors have studied this problem using *aggregation functions*, converting the multi-objective problem into a single objective one that assumes a (weighted or not) sum of the selected objective functions [23–30]. The major difficulty in this kind of problem consists in the incompatibility of different criteria. To create a global function, all criteria must be converted to the same measurement unit; a frequently used method is to convert them into costs, which is usually a tricky and often inaccurate operation. In addition, subjectivity appears, caused by the introduction of weighting factors for different criteria. Thus, the existence of a model that could take into

consideration more objective functions and constraints at the same time is of great interest. To eliminate the subjectivity and rigidity of the classic methods, the authors propose an original approach to formulate this problem using the *Pareto optimality* concept that defines a dominate relation among solutions.

Regardless of the problem formulation, *searching for the solution* is also a very complex issue due to its combinatorial nature. An absolute (e.g., “brute force” [10]) method which generates the entire space of candidate solutions in order to choose the best one, requires a prohibitive execution time. In order to avoid the evaluation of the entire space of the candidate solutions and to minimize the computation burden, several algorithms have been developed. Most authors have used different well known heuristics (branch exchange [2,3,21], branch and bound [1,4], simulated annealing [5]), other heuristic rules or meta-heuristics [7–9,11–13,15,17,22,23,25,27,28] or multi-agent technologies [20]. On the other hand, some authors have developed methods based on evolutionary computation techniques [6,14,16,18,19,24,26,29,30]. An important drawback of these methods is the fact that *they solve the reconfiguration problems as single objective problems*. Nevertheless, some authors have proposed Pareto optimality based approaches (including active power losses and reliability indices as objectives). With these approaches, linear programming cannot be used because we have more than one objective function. Thereby, different artificial intelligence based methods have been used: evolutionary [31], branch exchange [32] and particle swarm optimization [33].

Taking into account these considerations, we can observe the fact that this problem is arduous particularly from two points of view: (i) *the formulation of the problem*, because there is more than one objective; (ii) *the search for the optimal solution*, because of the prohibitive execution time demanded by applying an absolute method. In this paper an original method, aiming the optimization through the reconfiguration of distribution systems, is proposed. The novelty of the method consists in:

- the criteria for optimization are evaluated on active power distribution systems (containing distributed generators connected directly to the main distribution system and microgrids operated in grid-connected mode);
- the original formulation of the optimization problem, as a Pareto optimal one, with two objective functions (*active power losses* and *system average interruption frequency index*);
- an original genetic algorithm (based on NSGA-II) to solve the problem (as a Pareto optimal one) in a non-prohibitive execution time.

2. Problem Formulation

2.1. Criteria for Optimization

2.1.1. Active Power Losses (ΔP)

Active power losses represent the most important criterion and cannot be ignored in reconfiguration problems [1–33]. In order to evaluate this criterion it is necessary to perform the load flow calculus. Basically, power flow algorithms are iterative and are based on different procedures: Gauss-Seidel, Newton-Raphson, backward/forward sweep. For distribution systems which are operated in radial configurations, the most recommended approaches are *backward/forward sweep* based algorithms.

Due to its accuracy, the relatively small iteration number required and its robust convergence, the version presented in [34] has been chosen (where the sources are modeled as PQ nodes).

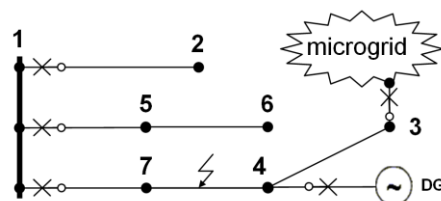
2.1.2. Reliability of the Distribution System

The essential attributes of interruptions in the power supply of the customers are the frequency and duration. While duration is predominantly influenced by the distribution system structure (radial, meshed, weak meshed) and the existing automations, the frequency is mainly influenced by the adopted operational configuration; it can be minimized by the suitable choice of the effective configuration. In other words, through reconfiguration, we can improve those reliability indices which refer to the interruption frequency [32]. Otherwise, the reliability of a distribution system can be considered from two different angles:

- Reliability of *a particular customer*: e.g., the average number of interruptions to the power supply. This index can represent a possible objective and/or constraint in the optimization problem (because some customers can impose maximal/minimal limits in their supply contracts);
- Reliability of *the entire supply system*: e.g., the number of interrupted customers *per year* [32], system average interruption frequency index (*SAIFI*) [35] (defined as: total number of customer interruptions longer than 3 minutes *per* total number of customers served).

For any fault that will lead to the interruption of the power supply from the main distribution system, the existing distributed generators will be switched off owing to a variety of reasons. We point out only two of them: (i) an operation of a power island purely with dispersed generators is usually considered unacceptable; (ii) it is important to *create conditions for auto-reclose of the main circuit breaker* (if this equipment is used in the distribution system). An exception appears if we have *microgrids* connected to the distribution network (which contains controllable loads, DG sources, storage devices, automations, *etc.*). In this case the consumers (loads) from the microgrid will be supplied even if a fault has occurred in the distribution system. For instance, if a fault occurred on the electric line 4–7 (Figure 1), the DG connected to node 4 and the microgrid connected to node 3 will be isolated (e.g., by *loss of mains protection* [36]). In this case, the microgrid is expected to operate as a power island (even if is necessary to operate the *automatic load-shedding control equipment*). The customers from the microgrid will be supplied even if a fault has occurred in the main distribution system because a microgrid must have both primary and secondary control algorithms [37].

Figure 1. A distribution smart grid with a distributed generator and a microgrid.



Knowing the failure rates at the level of each supplied node (load point), we can estimate the *SAIFI* using the relationship (in a similar form to the one given in [38]):

$$SAIFI = \frac{\sum_{i=1}^n \lambda_{ti} \cdot N_i}{N} \cdot T \quad (1)$$

where N represents the total number of customers served; N_i is the total number of customers supplied from node i ; T is the reference period [*year*], ($T = 1$ *year*); n is the number of load nodes of the system; λ_{ti} is the total failure rate of the equivalent element corresponding to the reliability block diagram at the level of node i [*year*⁻¹].

The total failure rate at the level of a node i (for a configuration) can be calculated as $\lambda_{ti} = \lambda_i + k \lambda_i'$, where λ_i is the failure rate when the restoring of supply is performed after the fault repair; while λ_i' is the failure rate when the restoring of supply is performed after the fault isolation through non-automatic maneuvers; and $k = [0, 1]$ is a coefficient that estimates the weight of restoring after 3 minutes (sustained interruption restored after fault isolation). In a first approximation, for reconfiguration studies, we consider $k = 1$, which corresponds to the most unfavorable case (when all restorations of supply after fault isolations through non-automatic maneuvers are performed after 3 minutes) [31]. It must be also specified that the contingencies are considered simple and the electric distribution system components are independent from the reliability point of view. A numerical example in order to explain how the *SAIFI* index is computed is given in what follows. Considering the sample system from Figure 1 we assumed that each branch has the failure rate $\lambda = 0.5$ [*year*⁻¹], on each supplied node there are 30 customers and the microgrid connected to node 3 (which contains 30 customers and DG units) behaves as a source. In this case we will have ($T = 1$ *year*):

- $N = 30 \cdot 6 = 180$ (six nodes, 30 customers for each node);
- $\lambda_{t2} \cdot N_2 = 0.5 \cdot 30 = 15$;
- $\lambda_{t3} \cdot N_3 = 0.5 \cdot 3 \cdot 0 = 0$ (three branches, the microgrid is expected to operate as an island and customers from a microgrid will be supplied even if a fault has occurred in the main distribution system);
- $\lambda_{t4} \cdot N_4 = 0.5 \cdot 3 \cdot 30 = 45$ (three branches, if a fault occurs on the path 1-7-4-3, the DG unit will be switched off and the customers will be not supplied);
- $\lambda_{t5} \cdot N_5 = \lambda_{t6} \cdot N_6 = 0.5 \cdot 2 \cdot 30 = 30$ (two branches);
- $\lambda_{t7} \cdot N_7 = 0.5 \cdot 3 \cdot 30 = 45$;
- $SAIFI = (15 + 0 + 45 + 30 + 30 + 45)/180 = 0.9167$.

2.1.3. Other Criteria

- *Node Voltages (V_i)*: Basically, each voltage r.m.s. value of the network nodes must be framed within the allowable limits.
- *Branch Load Limits through Lines (I_{ij})*: a typical constraint on the reconfiguration problem.
- *Safeguard of power supplies for all customers*: The attached graph of the electric system should be connected (a tree or a forest).
- *Configuration of the Distribution System*: Generally, electrical distribution systems are operated in radial configuration. This condition can be expressed as follows:

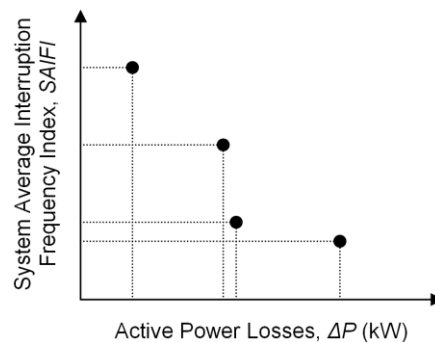
$$\sum_{ij \in E} \alpha_{ij} = n - p \tag{2}$$

where α_{ij} is a binary variable, representing the status of a tie line (0–open, 1–closed); n is the number of electric system nodes; E is the set of power system lines (branches) and p is the number of *connected components*. In graph theory terms, for a system with one source ($p = 1$) we are talking about an *optimal tree* and for a system with more than one feeder ($p > 1$) we are talking about an *optimal forest* with a number of trees (connected components) equal to that of source nodes.

2.2. Pareto Optimality Problem Formulation

The criteria presented above are not unique, but we consider them to be the most important ones. Taking into account these criteria, we can begin to perceive the real dimensions of the problem. These criteria are incompatible from the point of view of measurement units and can be grouped in two different categories: *objective functions* and *constraints (restrictions)*. In Pareto optimization, the central concept is named *non-dominated solution*. This solution must satisfy the following two conditions: (i) there is no other solution that is superior at least in one objective function; (ii) it is equal or superior with respect to other objective function values. Usually, the solution is not unique and consists of a set of acceptable optimal solutions (Pareto optimal). The set of Pareto solutions forms the *Pareto front* associated with a problem. Figure 2 presents a possible Pareto front for the optimization problem based on two objectives (ΔP and *SAIFI*). The Pareto front allows an informed decision to be made by visualizing an extensive range of options since it contains the solutions that are optimal from an overall standpoint.

Figure 2. A Pareto front for a bi-objective reconfiguration problem.



As a Pareto optimal multi-objective problem, we propose the following form:

Objective function

$$\min[\Delta P, SAIFI] \tag{3}$$

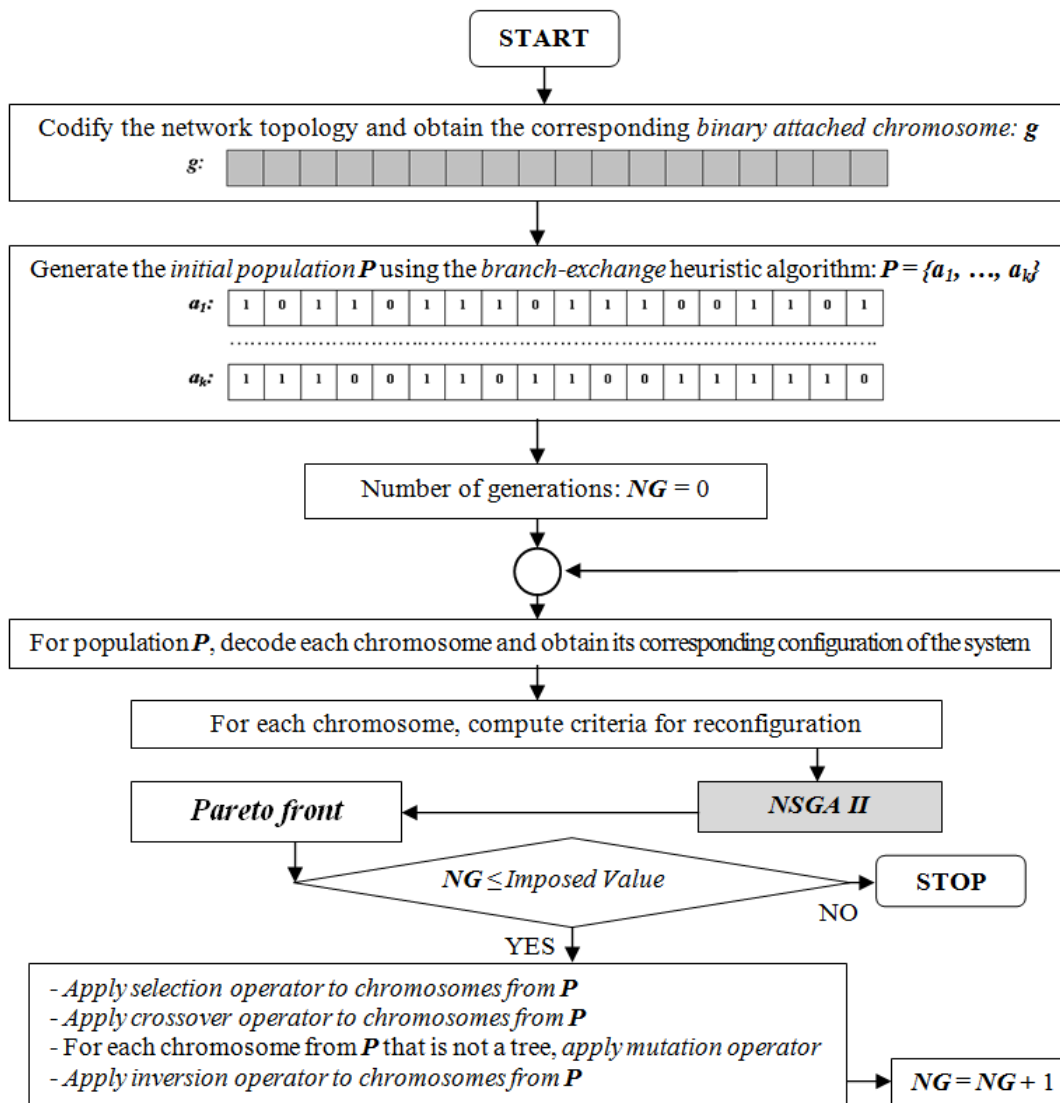
Constraints

$$\begin{aligned} V_i^{\min} &\leq V_i \leq V_i^{\max} \\ I_{ij} &\leq I_{ij}^{\max} \\ \sum_{ij \in E} \alpha_{ij} &= n - p \end{aligned} \tag{4}$$

3. Problem Solving

In the case of multi-objective problems, the literature proposes several Pareto-based genetic algorithms: *MOGA* (Multi Objective Genetic Algorithm) [39], *NPGA* (Niche Pareto Genetic Algorithm) [40], *SPEA/SPEA-II* (Strength Pareto Evolutionary Algorithm) [41], and *NSGA/NSGA-II* (Non-dominated Sorting Genetic Algorithm) [42]. After experimental comparison of these algorithms, the authors have decided to solve the multi-objective optimization problem through reconfiguration by using the *NSGA-II* algorithm with significant results (optimal solutions in short execution times). The logical diagram of the proposed *NSGA-II* based algorithm (*MOReco*–Multi Objective Reconfiguration) is given in Figure 3. The *initial population* is generated using the *branch-exchange* heuristic algorithm presented in [3]. A potential solution is selected only if all considered constraints are satisfied.

Figure 3. Logical diagram of the proposed algorithm (*MOReco*) dedicated to the reconfiguration of power distribution systems.

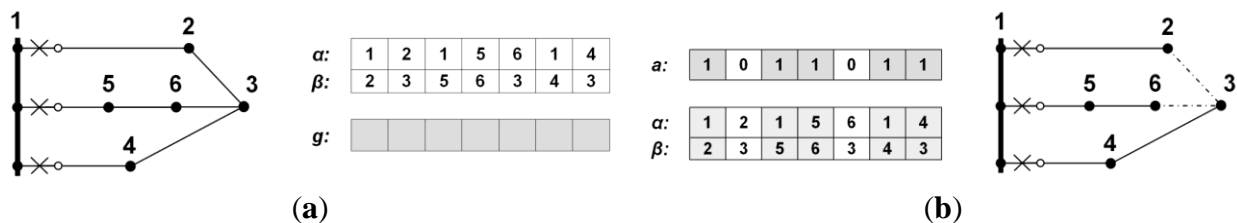


3.1. Genetic Encoding and Decoding of Power Distribution System Topology

3.1.1. Genetic Encoding

In this implementation, the representation using the *branch lists* was chosen because a power system node is only linked with a small part of the other nodes (it results in a rare graph, *i.e.*, the associated matrix contains many zero elements). Consequently, the graph associated with the electric network can be described by a matrix with 2 lines and *m* columns (where *m* is the number of the branches), each column indicating the two ends of a branch. This matrix does not contain zero elements. Therefore, using the representation via the branch lists, a binary codification of the problem (binary chromosome with fixed length) can be obtained. Binary values of the chromosome will indicate the status of every electric line: 0–open, 1–closed. Figure 4a exemplifies the graph (which indicates the network topology) attached to a distribution system, represented by branch lists (α and β), and the binary attached chromosome *g* (system/grid encoding).

Figure 4. A power distribution system: (a) the branch lists of the attached graph (α and β) and the attached chromosome (*g*); (b) Branch lists (α and β) obtained by decoding the chromosome *a*.



3.1.2. Genetic Decoding

The operation scheme of the system will be obtained by making the preservation of the corresponding branch value equal 1 (in operation). For instance, by decoding the chromosome *a*, the radial operation scheme will be obtained (with corresponding α and β lists) (Figure 4b). Using this codification, we have a population that consists of a set of chromosomes of type *a*. By decoding each chromosome, a particular configuration will be obtained and its performance can be tested.

3.2. Genetic Operators

3.2.1. Selection

The goal of the selection operator is to assure more chances to replicate for the best chromosomes of a population. The selection is performed taking into account the fitness of the chromosomes. The most used selection methods are Monte Carlo and tournament. For this multi-objective optimization problem, the author has used the ecological niche method [43].

3.2.2. Crossover

Choosing the number and position of crossover points for the crossover operator depends on the system topology. If these points are selected in an inadequate mode we will obtain “bad” chromosomes: (i) un-connected systems with isolated nodes; or (ii) connected systems with loops (meshed). In order to reduce the number of these cases, we propose that the number of cut points be equal to $CN - 1$. CN represents the cyclomatic number (the number of fundamental circuits/loops) corresponding to the attached graph: $CN = m - n + p$ (where m is the number of branches, n is the number of nodes/vertices and p is the number of connected components).

3.2.3. Mutation

One of the two conditions in order to have a tree or a forest is to assure $n-p$ closed branches (in operation), as in relationship (2). A radial configuration cannot be converted to another radial one by simply altering the value of a chosen gene. Therefore, we use this operator only in the case when, by performing the crossover operator, non-radial configurations are obtained. Thus, if in a chromosome there are more or fewer than $n-p$ genes equal to 1, the mutation operator randomly replaces the excess/insufficiency of genes equal to 1 (in order to have $n-p$ genes equal to 1).

3.2.4. Inversion

The second condition in order to have a tree or a forest is to have a connected graph (*for a tree*) or a graph with connected components (*for a forest*). Thus, this operator makes some branch-exchanges (each inversion between two genes of a chromosome behaves as a branch-exchange), repairing existing non connected graph chromosomes (which are not connected but which have $n-p$ genes equal to 1) and increases the diversity of a population. In our algorithm, this is an intensively used operator after performing crossover and mutation.

4. Simulation Results

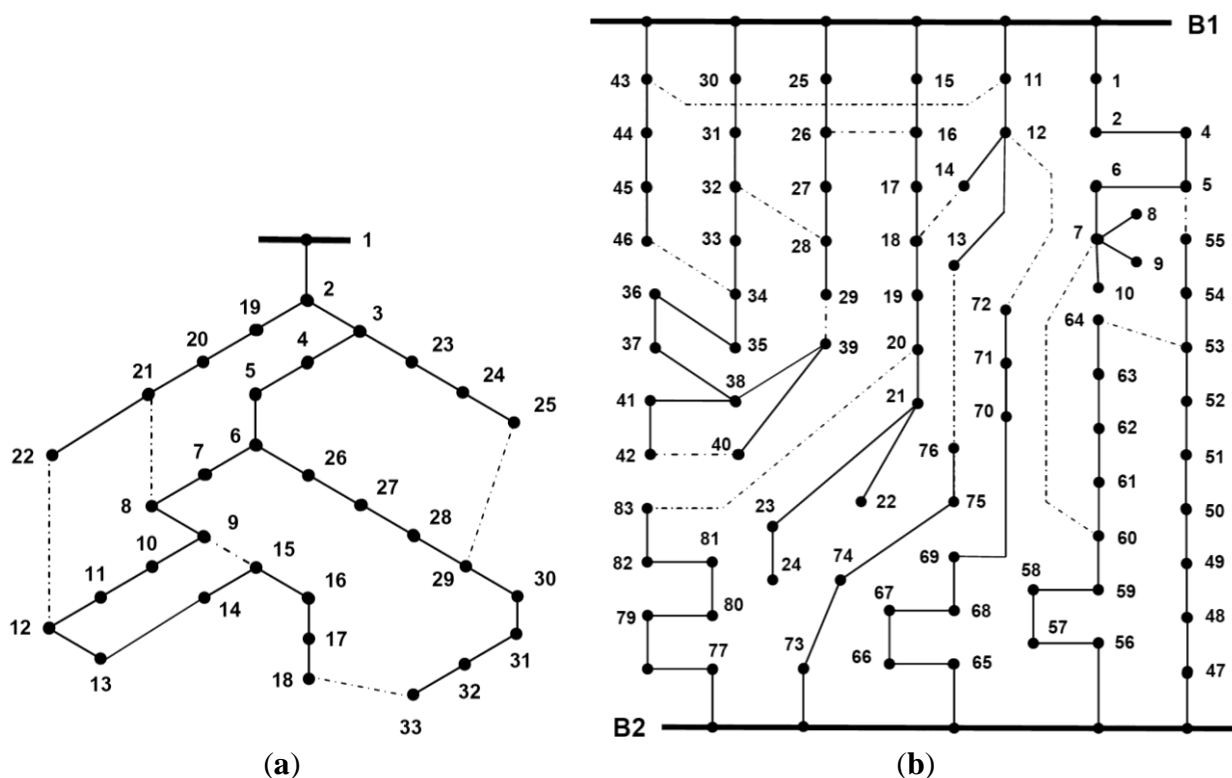
The Pareto front allows an informed decision to be made by visualizing an extensive range of options since it contains the solutions that are optimal from an overall standpoint. The proposed algorithm was implemented in the C++ programming language. The implementation was adapted in order to work with one objective (ΔP) and with two objectives (ΔP and $SAIFI$). Thus, the user can choose (in a flexible mode) ΔP as the objective function and some criteria as constraints (voltage deviation, loads limits through lines, *etc.*) or a vector objective function with ΔP and $SAIFI$ as variables (at the same time) and other criteria as constraints. The stopping criterion of the algorithm is an imposed maximum number of generations. All tests were performed on a PC equipped with an Intel Core Duo (3 GHz) processor and 4 GB of memory. Validation of the proposed algorithm implementation has been a difficult process especially because of the load flow computation unit. Data regarding different quantities (active power losses, voltages nodes) have been presented in literature in a variety of forms (*p.u.*, actual values or a mixture) and there are some approximations caused by the load flow algorithm which was used. E.g., in case [2], before the reconfiguration (in the base case), the total active power losses are 0.00511 *p.u.* After reconfiguration (by applying the MORECO algorithm),

the total active power losses are 0.004658 *p.u.* This result represents the optimal configuration and is confirmed in [9] and [11]. Another example is given in [5]. Before the reconfiguration, the total active power losses are 20.87 kW. This value is different from the 69.76 kW value which was presented in [5]. After reconfiguration, the total active power losses are 9.43 kW. These results are confirmed in [16].

In order to test the correctness and convergence speed of the proposed algorithm, the authors studied, first of all, five well known *single-objective* (active power losses) test systems. Table 1 presents two *single-objective* (active power losses) test cases where power distribution systems contain distributed generation:

- *System A* (Figure 5a) [3,27]: There are four DG units installed on nodes 3, 6, 24 and 29 [27]. In the base case, the total active power losses are 169.881 kW. By applying *MOREco* algorithm (after reconfiguration), the total active power losses are 115.748 kW. The evolution of the active power losses along the searching process is presented in Figure 6a.
- *System B* (Figure 5b) [27]: In this case, there are eight DG units installed on nodes: 7, 12, 19, 28, 34, 71, 75 and 79 [26]. Before the reconfiguration, the total active power losses are 425.131 kW (as in [26]). After reconfiguration, we obtained a better configuration than the one presented in [26]. The total active power losses are 380.656 kW, therefore smaller than 383.524 kW. The evolution of the active power losses along the searching process is presented in Figure 6b.

Figure 5. Test distribution systems: (a) system A [3]; (b) system B [27].



The proposed algorithm has an excellent behavior obtaining good quality solutions in reduced computation times (seconds); usually, a reduced number of generations is necessary for convergence. Performing reconfiguration for the test system B [27] as a Pareto problem, the operating configurations are obtained by optimizing two criteria: ΔP and *SAIFI* (Table 2). The Appendix indicates the failure

rates of branches considered in reconfiguration calculus. It is assumed that each node has three supplied consumers. In these study cases we considered two scenarios:

Figure 6. The evolution of the active power losses along the searching process (in the case of minimum CPU runtime): (a) for test distribution system A with DGs; (b) for test distribution system B with DGs.

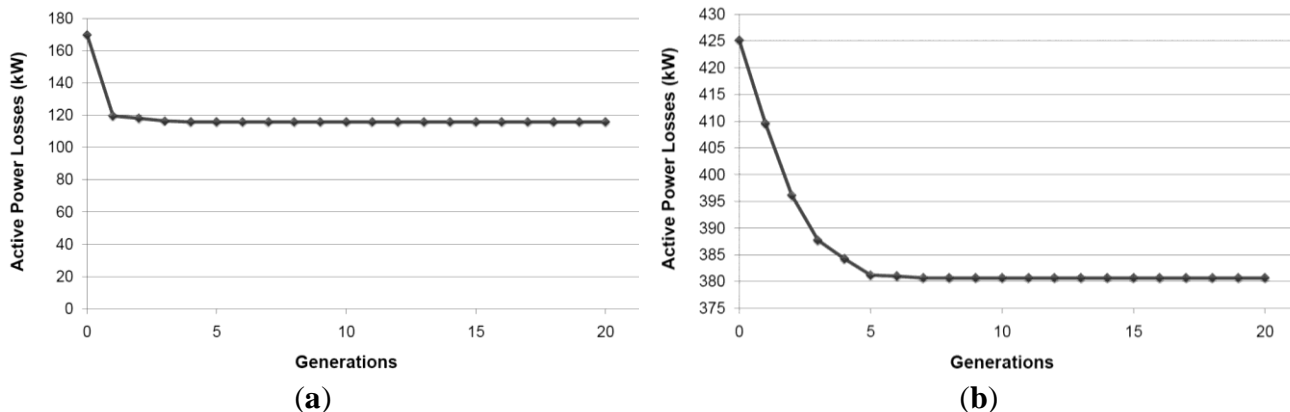


Table 1. Results for different single-objective reconfiguration (test cases with DGs).

System	Configuration	Open branches (tie lines)	Active power losses	CPU runtime for 100 runs	Population/Generations
A	Base case	8–21, 9–15, 12–22, 18–33, 25–29	169.881 kW	-	
	MOReco	7–8, 9–10, 14–15, 28–29, 32–33	115.748 kW	Minimum (3 s: 804 ms) Maximum (3 s: 974 ms) Average (3 s: 910 ms)	10/4
B	Base case	5–55, 7–60, 11–43, 12–72, 13–76, 14–18, 16–26, 20–83, 28–32, 29–39, 34–46, 40–42, 53–64	425.131 kW	-	
	MOReco	6–7, 12–13, 32–33, 38–39, 41–42, 54–55, 62–63, 71–72, 82–83, 11–43, 14–18, 16–26, 28–32	380.656 kW	Minimum (6 s: 202 ms) Maximum (7 s: 108 ms) Average (6 s: 675 ms)	10/8

Table 2. Results for Pareto reconfiguration with two objectives.

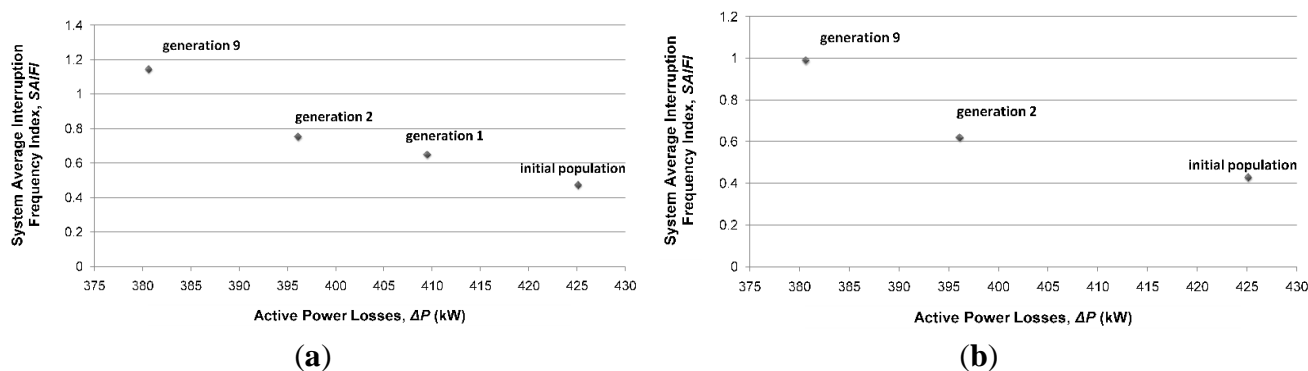
System	Open branches (tie lines)	Active power losses	SAIFI	CPU runtime for 100 runs	Population/Generations
B with DGs	6–7, 12–13, 32–33, 38–39, 41–42, 54–55, 62–63, 71–72, 82–83, 11–43, 14–18, 16–26, 28–32	380.656 kW	1.143	Minimum	10/9
	5–55, 6–7, 11–43, 12–72, 13–76, 14–18, 16–26, 20–83, 28–32, 29–39, 32–33, 40–42, 53–64	396.143 kW	0.751	(6 s: 952 ms) Maximum	-
	5–55, 6–7, 11–43, 12–72, 13–76, 14–18, 16–26, 20–83, 28–32, 29–39, 34–46, 40–42, 53–64	409.526 kW	0.648	(7 s: 279 ms) Average	-
	5–55, 7–60, 11–43, 12–72, 13–76, 14–18, 16–26, 20–83, 28–32, 29–39, 34–46, 40–42, 53–64	425.131 kW	0.472	(7 s: 40 ms)	-

Table 2. Cont.

System	Open branches (tie lines)	Active power losses	SAIFI	CPU runtime for 100 runs	Population/Generations
B with microgrids	6–7, 12–13, 32–33, 38–39, 41–42, 54–55, 62–63, 71–72, 82–83, 11–43, 14–18, 16–26, 28–32	380.656 kW	0.988	Minimum (7 s: 114 ms)	10/9
	5–55, 6–7, 11–43, 12–72, 13–76, 14–18, 16–26, 20–83, 28–32, 29–39, 32–33, 40–42, 53–64	396.143 kW	0.619	Maximum (7 s: 342 ms)	-
	5–55, 7–60, 11–43, 12–72, 13–76, 14–18, 16–26, 20–83, 28–32, 29–39, 34–46, 40–42, 53–64	425.131 kW	0.427	Average (7 s: 171 ms)	-

- *System B with DG units*: The proposed algorithm has obtained a Pareto front with four solutions (Figure 7a). In this case, the first non-dominated solution was obtained from initial population. After the first generation, the algorithm found the second non-dominated solution (the Pareto front contains two solutions). The searching process continued and the third non-dominated solution was found in generation 2 (at the end of generation 2, the Pareto front contains three solutions). The searching process continued, but without finding other non-dominated solutions until generation 9, where the fourth and final non-dominated solution was found. In the end, the Pareto front contains four non-dominated solutions.
- *System B with microgrids* (instead of DG units, as sources on the points of common coupling): The proposed algorithm obtained a Pareto front with three solutions (Figure 7b). As in the previous case, along the searching process, the Pareto front increases from one solution (from the initial population), to two solutions (generation 2) and, finally, to three solutions (in generation 9). We can observe that the *SAIFI* index is smaller in the case of existing microgrids than in the case where we consider just distributed generators.

Figure 7. The Pareto front (in the case of minimum CPU runtime): (a) for system B with DG units; (b) for system B with microgrids.



It is important to mention the fact that, in the case of the proposed algorithm, we obtained the same results for 100 runs. The differences consist only in the execution time required (e.g., between 6 s: 952 ms and 7 s: 279 ms, for the test case B with DGs, Table 2, where multi-objective reconfiguration is done), especially because of the inversion operator (applied a random number of times). There are different execution times in a generation and an important advantage: a large *breadth search* and a convergence to optimum in a reduced number of generations.

The proposed algorithm tries to exploit the fundamental properties of a distribution system, *i.e.*, to have a radial configuration in operation. It tries to generate just radial configurations (by using the branch exchange heuristic procedure to generate the initial population and by crossover operator.) By choosing the number of cut points equal to the cyclomatic number -1 , usually, other valid chromosomes are obtained, increasing the diversity of the population. This implementation does not ensure just valid chromosomes because in some cases, non-valid chromosomes (non radial configurations) are obtained. However, in combination with the mutation, this disadvantage is transformed into an important advantage because the diversity of the population is substantially increased and new zones from the research space are explored. Not ultimately, the implemented inversion operator, applied a random number of times to the chromosomes, expands the search space enough in order to find a good solution in a reduced number of generations.

5. Conclusions

Reconfiguration represents one of the most important measures which can improve the performance in the operation of a distribution system. Optimization through the reconfiguration (or optimal reconfiguration) of a power distribution system is not a new problem but still represents a difficult one and nowadays has new valences. Besides active power losses, the average number of interruptions to the power supply represents an essential criterion which must be taken into consideration in the optimization problem. The criteria for optimization have been evaluated on active power distribution systems (containing distributed generators connected directly to the main distribution system and microgrids operated in grid-connected mode). The simulation studies on test systems have highlighted that the *SAIFI* index is smaller in the case of existing microgrids (because the consumers which are inside the microgrid are supplied even if a fault has occurred in the main distribution system) than in the case of distributed generators connected directly to the main distribution system.

The original formulation of the optimization problem, as a Pareto optimal one, with two objective functions (*active power losses* and *system average interruption frequency index*) ensures an objective and robust solution. Thus, the weak points of the classic methods proposed in literature can be eliminated; we are especially talking about: (i) errors caused by the conversion of different objective functions into the same measurement units; and (ii) the subjectivities caused by the introduction of weighting factors for different criteria.

Usually, the existing reconfiguration methods used nowadays either demand prohibitive execution times or result in non-optimal solutions (in the case of most common heuristics). The authors propose an original genetic algorithm (based on NSGA-II) to solve the problem (as a Pareto optimal one) in a non-prohibitive execution time. The comparative tests performed on some active test systems have demonstrated the accuracy and promptness of the proposed algorithm.

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Appendix

Table A1. Failure rates of system B (Figure 5b).

Branch	<i>i</i>	<i>j</i>	λ [<i>year</i> ⁻¹]	Branch	<i>i</i>	<i>j</i>	λ [<i>year</i> ⁻¹]	Branch	<i>i</i>	<i>j</i>	λ [<i>year</i> ⁻¹]
1	B1	1	0.071	37	36	37	0.016	73	B10	73	0.019
2	1	2	0.096	38	37	38	0.024	74	73	74	0.082
3	2	3	0.078	39	38	39	0.064	75	74	75	0.009
4	3	4	0.035	40	39	40	0.065	76	75	76	0.091
5	4	5	0.065	41	38	41	0.095	77	B11	77	0.065
6	5	6	0.082	42	41	42	0.046	78	77	78	0.017
7	6	7	0.059	43	B6	43	0.085	79	78	79	0.017
8	7	8	0.012	44	43	44	0.075	80	79	80	0.091
9	7	9	0.012	45	44	45	0.062	65	B9	65	0.042
10	7	10	0.011	46	45	46	0.036	66	65	66	0.054
11	B2	11	0.007	47	B7	47	0.065	67	66	67	0.017
12	11	12	0.039	48	47	48	0.093	68	67	68	0.016
13	12	13	0.095	49	48	49	0.019	69	68	69	0.085
14	12	14	0.036	50	49	50	0.065	70	69	70	0.066
15	B3	15	0.048	51	50	51	0.017	71	70	71	0.052
16	15	16	0.076	52	51	52	0.017	72	71	72	0.052
17	16	17	0.023	53	52	53	0.051	73	B10	73	0.019
18	17	18	0.094	54	53	54	0.026	74	73	74	0.082
19	18	19	0.056	55	54	55	0.055	75	74	75	0.009
20	19	20	0.067	56	B8	56	0.026	76	75	76	0.091
21	20	21	0.099	57	56	57	0.017	77	B11	77	0.065
22	21	22	0.045	58	57	58	0.032	78	77	78	0.017
23	21	23	0.073	59	58	59	0.017	79	78	79	0.017
24	23	24	0.046	60	59	60	0.068	80	79	80	0.091
25	B4	25	0.049	61	60	61	0.055	84	5	55	0.052
26	25	26	0.062	62	61	62	0.061	85	7	60	0.051
27	26	27	0.066	63	62	63	0.098	86	11	43	0.072
28	27	28	0.059	64	63	64	0.017	87	12	72	0.061
29	28	29	0.099	65	B9	65	0.042	88	13	76	0.069
30	B5	30	0.034	66	65	66	0.054	89	14	18	0.049
31	30	31	0.114	67	66	67	0.017	90	16	26	0.036
32	31	32	0.074	68	67	68	0.016	91	20	83	0.045
33	32	33	0.065	69	68	69	0.085	92	28	32	0.066
34	33	34	0.059	70	69	70	0.066	93	29	39	0.085
35	34	35	0.025	71	70	71	0.052	94	34	46	0.061
36	35	36	0.026	72	71	72	0.052	95	40	42	0.042

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