Abstract: Although tectonic areas with facies change (i.e., variation of coal seam thickness, coal seam dip angle, or coal quality) are one of the three major geological structures that induce rock bursts, case studies of rock bursts in these tectonic structures are rare. The main objective of this study is to illustrate this issue and provide case studies that may inspire future research. Based on several typical cases of rock bursts induced by tectonic areas with facies change, the conditions conducive for these bursts are introduced and investigated in detail. Subsequently, numerical simulation is performed, showing that stress concentration exists in regions with variable coal seam thicknesses or dip angle. When stoping or tunnelling approaches this region, the peak stress increases rapidly. Thus, the burst occurs via a mechanism involving the superposition of high in-situ stress from tectonic areas with facies change and abutment pressure from stoping or tunnelling, leading to high stress concentration. Strategies for mitigating rock bursts are also provided. Rock bursts induced by tectonic areas with facies change can be mitigated by avoiding regions of high tectonic stress concentration and reducing mining induced stress.

Keywords: geology; rock burst; tectonic area; mechanism; case histories

1. Introduction

Rock burst are common dynamic disasters that occur during underground mining [1–7]. Although scholars have focused on this issue for several decades, the mechanisms of rock bursts remain inadequately understood. It is generally acknowledged that geological structures including folds, faults, and tectonic areas with facies change contribute to the occurrence of rock burst hazards and other dynamic disasters [8–12]. According to incomplete statistics, rock bursts induced by geological structures account for nearly 70% of the total rock burst occurrences in China [13]. Extensive studies have been performed regarding the occurrence of rock bursts induced by geological structures. For fault induced rock bursts, Jiang et al. [14] and Li et al. [15] used FLAC3D numerical software to study the fault activation, and Dou et al. [16] investigated fault-slip rock bursts comprehensively via theoretical analysis, laboratory tests, numerical simulation, and engineering practice. Sainoki and Mitri [17] studied the dynamic behaviour of fault slips influenced by mining activities, and Hu et al. [18] developed a mechanical model of fault slipping. For fold-induced rock bursts, Wang et al. [19] and Chen et al. [20] studied the stress distribution in the core of the fold using numerical simulation.

Mining in tectonic areas with facies change (Figure 1) can easily cause dynamic disasters. However, limited literature is available regarding the underlying mechanisms. For example, Sun et al. [21]
studied 14 rock bursts related to the variation of coal seam thickness, and Zhai et al. [22] found that the variation of coal seam thickness was significantly correlated to coal and gas outbursts, and concluded that when the coal seam thickness suddenly increases, the gas content and the associated pressure continually increase. Case studies on the matter are important and valuable, but only a few recorded histories and experiences of rock bursts caused by tectonic areas with facies change have been reported. The literature on related mechanisms is rare except for a few studies on the variation of coal seam thickness. For example, Zhao et al. [23] studied mechanism of rock bursts induced by the variation of coal seam thickness, showing that stoping from thin to thick coal seams was beneficial for controlling rock bursts. In general, research attention for these kinds of rock bursts remains insufficient.

![Figure 1. Tectonic areas with facies change. (a) Variation of coal seam thickness, (b) variations of coal seam dip angle and coal quality [13].](image)

Therefore, to provide some references for studying the burst mechanism induced by tectonic areas with facies change, case studies of rock bursts related to the aforementioned geological structures are analyzed first. The occurrence conditions are introduced and investigated in detail. Subsequently, the occurrence mechanism of these rock bursts is discussed using FLAC3D simulation. Finally, suggestions for mitigating rock bursts induced by tectonic areas with facies change are provided for reference in further studies regarding burst mitigation.

2. Case Histories of Rock Bursts Related to the Variation of Coal Seam Thickness

2.1. Rock Burst in Mine A

A region with variation in the coal seam thickness was present in the central area of the headgate of W-No.1 mining face in Mine A, which was approximately 700 m deep. The variation of the coal seam thickness was 1.8–3.5 m with an average value of 2.9 m. The variation of the dip angle was 11–14° with an average dip angle of 12°. The floor, the immediate roof, and the main roof were composed of sandstone and fine siltstone with an average thickness of 4, 3, and 20 m, respectively. The minimum, the median, and the maximum principal stresses were 9.8, 19.6, and 23.1 MPa, respectively. The region of interest was in the plane of $\sigma_1$ and $\sigma_3$ [13]. On 28 June 2009, when the longwall face was 140 m away from the uphill roadway, a rock burst occurred at the headgate. This burst caused damage to the headgate 17 m in length with rib spalling 0.8–1.2 m thick. Additionally, the burst influenced the longwall face, which was 33 m in length. The burst site and damage photos are shown in Figure 2.
The rock burst region at the No. 1305 mining face was already in a high stress state due to its deep burial depth. The open-off cut of No. 1305 mining face was selected in a region with variable coal seam thickness, primarily due to a lack of awareness regarding rock bursts induced by variable coal seam thickness. When stoping began, the stress soon reached a critical value because of the additional abutment pressure, self-weight, and mining disturbances, resulting in a rock burst. It should be noted that no mitigation methods were implemented before the occurrence of this rock burst.

2.2. Rock Burst in Mine B

The buried depth of the No. 1305 mining face in Mine B, a typical mining face in the region with variable of coal seam thickness, was approximately 980 m. The variation in the coal seam thickness was 2.1–8.6 m with an average value of 6.02 m. The variation in the dip angle was 0–11° with an average dip angle of 3°. The floor, the immediate roof, and the main roof were composed of mudstone, siltstone, and medium sandstone, with average thicknesses of 1.7, 2.8, and 8.3 m, respectively. An intense rock burst occurred at the No. 1305 mining face when beginning to stope on 29 July 2015, as illustrated in Figure 3a. The rock burst damaged the entire longwall face, 60 m long tailgate, and the 40 m long headgate, including floor heave, roof fall, support bending, and coal cutter damage, as shown in Figure 3b,c.

A region with obviously variable coal seam thickness passes through this rock burst region. The rock burst region at the No. 1305 mining face was already in a high stress state due to its deep burial depth. The open-off cut of No. 1305 mining face was selected in a region with variable coal seam thickness, primarily due to a lack of awareness regarding rock bursts induced by variable coal seam thickness. When stoping began, the stress soon reached a critical value because of the additional abutment pressure and tectonic stress, resulting in the rock burst. In practice, the open-off cut should be located in a general area without high tectonic stress to prevent such disasters.
3. Case Histories of Rock Bursts

### 3.1. Rock Burst in Mine D

On 18 May 2013, a rock burst occurred in the downhill roadway on the east LW2302S mining face in Mine C, as illustrated in Figure 4. The buried depth was >900 m, and above the mining face was a 600 m thick alluvium stratum. This rock burst destroyed a 150 m long roadway, including server floor heaves and roof falls. A facies change belt, which assisted in the formation of variable coal seam thickness, crossed the rock burst region, indicating that the area was in a state of high tectonic stress. The roadway was also influenced by the abutment pressure on the LW2302S mining face [24], achieving the critical stress required for the rock burst in the red zone. However, this event could have been mitigated or prevented if appropriate measures were taken in the region with variable coal seam thickness before stoping.

![Figure 3](image1.png)

**Figure 3.** Rock burst region in the No. 1305 mining face and photos of the rock burst damage, (a) rock burst region, (b) roadway damage, (c) longwall face damage.

### 2.3. Rock Burst in Mine C

On 18 May 2013, a rock burst occurred in the downhill roadway on the east LW2302S mining face in Mine C, as illustrated in Figure 4. The buried depth was >900 m, and above the mining face was a 600 m thick alluvium stratum. This rock burst destroyed a 150 m long roadway, including server floor heaves and roof falls. A facies change belt, which assisted in the formation of variable coal seam thickness, crossed the rock burst region, indicating that the area was in a state of high tectonic stress. The roadway was also influenced by the abutment pressure on the LW2302S mining face [24], achieving the critical stress required for the rock burst in the red zone. However, this event could have been mitigated or prevented if appropriate measures were taken in the region with variable coal seam thickness before stoping.

![Figure 4](image2.png)

**Figure 4.** Rock burst region in the LW2302S mining face [24].
3. Case Histories of Rock Bursts Related to the Variation of Coal Seam Dip Angle

3.1. Rock Burst in Mine D

On 5 August 2013, an intense rock burst occurred behind the 200 m long heading face in the No. 3302 mining face while tunnelling the tailgate in Mine D, as shown in Figure 5a [25]. This rock burst destroyed the nearly 150 m long roadway. Figure 5b,c shows images of the related burst damage. This was the first mining face and was buried 1260 m deep. The average coal seam thickness and dip angle were approximately 9 m and 8°, respectively. The roof was composed of 5–20 m thick sandstone. Figure 5a shows that the rock burst occurred in the region with variable coal seam dip angles. In other words, the observations indicated that the variable coal seam dip angle likely contributed to this rock burst.

![Figure 5](image)

**Figure 5.** Rock burst region in the No. 3302 mining face and photos of the associated rock burst damage [25]. (a) rock burst region, (b) roadway damage

3.2. Rock Burst in Mine E

The buried depth of the No. 2 mining face in Mine E was >1000 m. The coal seam thickness varied from 0.3 to 2.7 m with an average thickness of 1.5 m. The dip angle varied from 12 to 29° with an average dip angle of 18°. The floor, the immediate roof, and the main roof were composed of siltstone and fine sandstone, whose corresponding thicknesses were 10–17, 11–13, and 17–33 m, respectively. The test results of in-situ stress in Mine E are listed in Table 1. The results showed that the stress state was in the plane of $\sigma_1$ and $\sigma_3$, and that horizontal stress was the dominant stress mode.

<table>
<thead>
<tr>
<th>Depth/m</th>
<th>Maximum Principal Stress ($\sigma_1$)</th>
<th>Median Principal Stress ($\sigma_2$)</th>
<th>Minimum Principal Stress ($\sigma_3$)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Value/MPa</td>
<td>Azimuth Angle/°</td>
<td>Dip Angle/°</td>
</tr>
<tr>
<td>672</td>
<td>26.30</td>
<td>224.00</td>
<td>14.50</td>
</tr>
<tr>
<td>510</td>
<td>20.50</td>
<td>252.00</td>
<td>-7.00</td>
</tr>
<tr>
<td>465</td>
<td>19.10</td>
<td>232.00</td>
<td>12.00</td>
</tr>
<tr>
<td>580</td>
<td>22.60</td>
<td>213.00</td>
<td>1.00</td>
</tr>
</tbody>
</table>
On 25 October 2016, a rock burst occurred at the junction between the open-off cut and tailgate under the influence of a blasting disturbance, as shown in Figure 6. This rock burst caused rib spalling of 0.1–0.3 m in width and failure of a few cables. When this event occurred, no mining activities were being performed, while the dip angle of coal seam varied from 18 to 37° in this region. Thus, it could be concluded that the variable dip angle most significantly contributed to this burst.

![Figure 6. Rock burst region in the No. 2 mining face.](image)

4. Case Histories of Rock Bursts Related to the Variation of Coal Quality

4.1. Rock Burst in Mine E

The buried depth of the No. 1 mining face in Mine E was >800 m. The variation of coal seam thickness was 0.6–2.2 m with an average value of 1.5 m. The variation of dip angle was 10–30° with an average dip angle of 16°. The floor, the immediate roof, and the main roof were composed of siltstone and fine sandstone with thicknesses of 10–17, 11–13, and 17–33 m, respectively. On 10 August 2016, a rock burst occurred in the uphill roadway near the No. 1 mining face during tunnelling, as shown in Figure 7. This rock burst caused a floor heave of 0.2–0.5 m in height and shifting of the transportation track.

![Figure 7. Rock burst region in the No. 1 mining face.](image)

The burst occurred in a region where the coal hardness changed, as shown in Figure 7. Because of the lack of knowledge of rock bursts induced by variation in coal quality, no mitigation methods were considered before tunnelling. When tunnelling in this region, the stress reached a critical value and caused the rock burst. This event could have been avoided if proper mitigation was implemented.
4.2. Rock Burst in Mine F

On 28 August 2011, a rock burst occurred behind the heading face 5–6 m in length in the No. 2302 mining face during tailgate tunnelling in Mine F, as illustrated in Figure 8. The variation of the coal seam thickness was 3.8–8.5 m with an average value of 7.7 m. The variation of the dip angle was 6.0–9.6° with an average value of 7.8°. This rock burst caused a few pieces of coal to be ejected, and the burst region was buried at a depth of 900 m. Figure 8 clearly shows that the distance between the burst region and fault was approximately 222 m, indicating that the region was not influenced by the fault. The field investigation showed that the coal on the left side of the heading face was harder than that on the right side. Fortunately, when mitigation methods were implemented on the left side, no further rock bursts occurred [27]. Therefore, it could be concluded that this rock burst was induced by variation in the coal quality.

![Figure 8. Rock burst region in the No. 1 mining face [26].](image)

5. Discussions

From the representative rock burst case studies in tectonic areas with facies change provided above, it can be concluded that when tunnelling or stoping approaches tectonic areas with facies changes, the critical stress required for rock bursts can easily be achieved. Therefore, tectonic areas with facies change require screening for both faults and folds. In this section, we discuss the mechanisms of rock bursts induced by tectonic areas with facies change and related mitigation suggestions.

5.1. Rock Burst Mechanism Induced by Tectonic Areas with Facies Change

Zhao et al. [23] showed that in-situ stress concentration and stress gradient zones are present in regions with variable coal seam thickness, as shown in Figure 9. In-situ stress in the thinning area was observed to be larger than that in the thickening area. The authors also found that larger variation amplitudes resulted in larger stress gradients. For example, when the coal seam thickness varied between 5 and 2 m, the value of variation amplitude was 6.3 MPa, while it was only 1.6 MPa when the coal seam thickness varied from 5 to 4 m.

![Figure 9. Cont.](image)
Coal seam dip angle with facies changes can be described as follows—in-situ stress concentration zones exist in critical areas (Figure 11a). When stoping or tunnelling approaches the in-situ stress concentration zones, these areas will experience high stress caused by the superposition of the high in-situ stress concentration from tectonic areas with facies changes and abutment pressure from stoping or tunnelling (Figure 11b), leading to rock bursts.

To further analyze the abutment pressure distribution during the stoping process in the variable coal seam thickness region, the abutment pressure distribution at different distances between the variable region (5–2 m) and longwall face is shown in Figure 9c. The stress concentration factor in the variable region showed an increasing trend with decreasing distance between the longwall face and the variable region. When the distance decreased from 20 to 5 m, the stress concentration factor in the variable region gradually increased from 1.39 to 1.89. If the peak abutment pressure stress approaches this region, stress superposition can easily occur, enhancing the risk of rock bursts.

Considering that the dip angles of the coal seam varied from 0° to 15–45°, seven numerical variation models of dip angles were established to study the in-situ stress distribution in this region, as shown in Figure 10a. The displacement boundary conditions, the constitutive model, and the mechanical properties of the coal, rock, etc. used in this simulation were similar to the available literature [23], except for the numerical model. The obtained in-situ stress distribution is shown in Figure 10b. From Figure 10b, it is clear that there was a stress concentration zone in the region with variable coal seam dip angles, and the stress concentration increased as the variable range of the dip angle increased.

Figure 10c shows the abutment pressure distribution at different distances between the variable region (0–30°) and the longwall face. The stress concentration factor in the variable region of the dip angle also showed an increasing trend with decreasing distance between the longwall face and the variable region. When the distance decreased from 20 to 5 m, the stress concentration factor in the variable region rapidly increased from 1.23 to 1.98. This indicated that when the longwall face approached the variable dip angle region, superposition of the abutment pressure and tectonic stress could easily occur, potentially inducing a rock burst.

For regions with variable coal quality, scholars have reached a consensus that under similar geological conditions, the in-situ stress of a hard coal seam is larger than that of a soft coal seam [27,28]. Similar stress concentration zones in regions with variable coal seam thicknesses and dip angles were also observed.

Based on the analysis of the in-situ stress distribution, a schematic of the rock burst mechanisms was generated and is shown in Figure 11. The mechanisms of rock bursts induced by tectonic areas with facies changes can be described as follows—in-situ stress concentration zones exist in critical areas (Figure 11a). When stoping or tunnelling approaches the in-situ stress concentration zones, these areas will experience high stress caused by the superposition of the high in-situ stress concentration from tectonic areas with facies changes and abutment pressure from stoping or tunnelling (Figure 11b), leading to rock bursts.

**Figure 9.** Numerical model of the variation of coal seam thickness, in-situ stress distribution, and abutment pressure distribution [23]. (a) numerical model of the variation of coal seam thickness, (b) distribution of the in-situ stress, (c) distribution of abutment pressure when stoping with coal seam thickness of 5 to 2 m.
Based on the case studies and determination of rock burst mechanisms, it is clear that rock bursts induced by tectonic areas with facies change can be mitigated by avoiding regions with high tectonic stress concentration and reducing mining-induced stress. Three basic suggestions for mitigating such rock bursts are proposed herein. First, when stoping or tunnelling, the roadway layout should avoid high tectonic stress concentration areas. Second, if tectonic areas with facies changes cannot be avoided while stoping or tunnelling, mitigation methods should be implemented more intensely than for areas not influenced by tectonic stress. Third, peak stress concentration areas should be thoroughly transferred into deep coal walls.
6. Conclusions

In this study, several cases of rock bursts related to tectonic areas with facies changes were analyzed in detail. Subsequently, the underlying mechanisms of these rock bursts as well as some mitigation strategies were discussed. The main conclusions are as follows:

(1) The rock burst case studies showed that tectonic areas with facies changes, including variations in coal seam thickness, coal seam dip angle, and coal quality, play an important role in tectonic rock bursts. Special attention should be paid to such rock bursts compared to those induced by the more widely studied faults and folds.

(2) Numerical simulation was used to investigate existing stress concentration in regions with variable coal seam thickness or dip angle. The stress concentration increases gradually as the variable range of coal seam thickness or dip angle increases. When stoping or tunnelling in these regions, the peak stress will increase rapidly.

(3) The superposition of high in-situ stress from tectonic areas with facies changes and abutment pressure from stoping or tunnelling leads to high stress concentration. Three main suggestions were provided for mitigating rock bursts induced by tectonic areas with facies changes. First, the roadway layout should avoid high tectonic stress concentration areas. Second, if stoping or tunnelling cannot avoid these sensitive areas, mitigation methods must be implemented. Third, peak stress concentration areas should be thoroughly transferred into deep coal walls.

Overall, this study aimed to highlight the issue of rock bursts induced by tectonic areas with facies changes for researchers interested in underground engineering and to provide case studies to inspire further research in this field.

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References


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