Microstructure, Texture Evolution and Magnetic Properties of Fe-6.5 wt. % Si and Fe-6.5 wt. % Si-0.5 wt. % Cu Alloys during Rolling and Annealing Treatment

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Abstract: Sheets of Fe-6.5 wt. % Si and Fe-6.5 wt. % Si-0.5 wt. % Cu with the thickness of 0.3 mm have been produced by hot and warm rolling. The microstructure, texture evolution and magnetic properties of the two alloys were investigated. It was found that the addition of 0.5 wt. % Cu promoted the formation of shear bands during warm rolling, and enhanced the \( \{110\}<001> \) texture at surface layer and \( \{111\}<112> \) texture in the middle layer. After annealing treatment, a strong \( \eta \) fiber texture with a peak at \( \{110\}<001> \) was formed in the Fe-6.5 wt. % Si-0.5 wt. % Cu sample, while the Fe-6.5 wt. % Si sample was characterized by complex \( \gamma \), \( \eta \) and \( \lambda \) fibers. The formation of dominating \( \eta \) fiber in the annealed Fe-6.5 wt. % Si-0.5 wt. % Cu sample is attributed to the shear bands formed in \( \{111\}<112> \) oriented grains. These shear bands in \( \{111\}<112> \) oriented grains acted as the nucleation sites of \( \eta \) oriented grains and promoted the growth of Goss oriented grains. The presence of strong \( \eta \) fiber with a peak at Goss in Fe-6.5 wt. % Si-0.5 wt. % Cu sample was the cause for the higher magnetic induction observed for this sample than for the Fe-6.5 wt. % Si sample.

Keywords: Fe-6.5 wt. % Si alloy; alloying; microstructure; texture evolution; magnetic properties

1. Introduction

Fe-6.5 wt. % Si alloy is regarded as an ideal material for energy efficient design and miniaturization of a diverse range of electrical devices because of its high electrical resistivity, high permeability and near zero magnetostriction [1,2]. Fe-6.5 wt. % Si alloy will meet the demands for energy loss reduction, improved efficiency and low noise during the process of electromagnetic transition [3]. However, it is almost impossible to cold-roll Fe-6.5 wt. % Si alloy into thin sheets for practical applications due to its near zero ductility. The brittleness of Fe-6.5 wt. % Si alloy at room temperature is caused mainly by the formation of the ordered phases such as B2 and D0\(_3\) in the microstructure [4,5]. In fact, commercial scale production of Fe-6.5 wt. % Si alloy sheets has only been successfully developed by JFE Steel Corporation (Tokyo, Japan) through a chemical vapor deposition (CVD) process [6]. However, the magnetic induction at 800 A/m (B\(_8\)) of the sheets with a thickness of 0.3 mm produced by CVD is about 1.27 T, which is much lower than the theoretical value of 1.8 T [7,8]. Therefore, the magnetic induction of Fe-6.5 wt. % Si alloy may potentially be improved by further optimizing its texture.

Ros-Yañez et al. [9] described the texture evolution in sheet steel. The texture after hot-rolling was composed of cube (\( \{001\}<100> \)), \( \gamma \) (\( \{111\} \) parallel to the rolling direction) and Goss (\( \{011\}<100> \)) components, which evolved to that consisting of strong \( \gamma \) and \( \lambda \) (\( <001> \) parallel to the normal direction) fibers after cold rolling, and finally to the one comprising \( \gamma \) fiber with a peak at \( \{111\}<110> \) after recrystallization. The recrystallization texture will depend on the heterogeneities in the texture after...
cold rolling. It is desirable to enhance the $\eta$ fiber ($<001>$ parallel to the rolling direction (RD)), and to suppress $\gamma$ fiber ($<001>$ not in the rolling direction). The $\eta$ and $\gamma$ recrystallized grains tend to nucleate mainly in shear bands and grain boundaries, respectively [10–12]. To improve the magnetic induction of Fe-6.5 wt. % Si sheets, many efforts have been focused on the formation of $\eta$ fiber. For instance, Liu et al. [13] studied the development of strong $\eta$ primary recrystallization texture in a 0.50 mm Fe-6.5 wt. % Si sheet produced by hot and cold rolling; Fang et al. [14] reported a recrystallization texture with a similar intensity of $\eta$ and $\gamma$ fibers in rolled 0.30 mm thick Fe-6.5 wt. % Si sheets by cold rolling; and Yao et al. [15] obtained $\eta$ fiber dominated recrystallization texture after high-temperature annealing (950–1150 °C) of a cold-rolled Fe-6.5 wt. % Si sheets of 0.2 mm thickness.

Our previous study [16] indicated that the addition of 0.5 wt. % Cu could increase the ductility of Fe-6.5 wt. % Si alloy at intermediate temperature (550 °C), as well as improving the magnetic properties after annealing at 1150 °C for 1 h. Nevertheless, there have been no studies on the detailed effect of Cu addition on the microstructure and texture evolution for the Fe-6.5 wt. % Si alloy, although Bian et al. [17] indicated that a suitable amount of Cu addition could improve the recrystallization textures of non-oriented silicon steel by inhibiting the $\{111\}$ component and promoting the Goss component. Thus, the focus of this paper is on the evolution of the microstructure and texture of Fe-6.5 wt. % Si and Fe-6.5 wt. % Si-0.5 wt. % Cu alloys during rolling and annealing processes.

2. Experimental Procedures

Two Fe-6.5 wt. % Si alloys, one without Cu and one with 0.5 wt. % Cu addition (labeled as 0Cu and 0.5Cu, respectively), were prepared by melting of iron (99.5 wt. %), silicon (99.5 wt. %) and copper (99.9 wt. %) in a vacuum induction furnace. The ingots were forged into slabs of about 20–30 mm thickness at 1100 °C, and then hot rolled to 0.8–1.0 mm at about 1000 °C. The hot-rolled sheets were further warm rolled to 0.3 mm at approximately 650 °C, and finally annealed at 900 °C for different times under a nitrogen–hydrogen ($N_2 + 50\% H_2$) atmosphere.

Optical microscopy (OM) (ZEISS, Jena, Germany) was used to observe the microstructure of samples. Textures of the warm-rolled sheets were quantitatively measured for the three incomplete pole figures $\{110\}$, $\{200\}$ and $\{112\}$ by X-ray diffraction (XRD, Mo$K_\alpha$ radiation, D/MAX-2500PC) (Bruker, Karlsruhe, Germany). The orientation distribution functions (ODFs) were then calculated from the pole figures by series expansion method ($I_{\text{max}} = 22$). The textures of the warm-rolled sheets were measured at the surface and in the middle layer, and the results were presented in the form of ODFs in the $\phi_2 = 45^\circ$ section. The formation of the recrystallization texture was analyzed by electron backscattered diffraction (EBSD) (Oxford Instruments, Oxford, UK, HKL Channel 5 EBSD equipped on the Nova 400 Nano field emission scanning electron microscope) (FEI, Hillsboro, OR, USA) operated at an accelerating voltage of 30 kV with a step of 0.6 µm. The microstructure and texture measurements were made on the longitudinal section defined by rolling direction (RD) and normal direction (ND). Moreover, the magnetic induction at 800 A/m ($B_8$) and 5000 A/m ($B_{50}$) of the sheets were measured by an AC/DC magnetic measuring instrument (MPG-100D) (Brockhaus, Lüdenscheid, Germany) with a sample size of 300 mm $\times$ 30 mm $\times$ 0.3 mm; the length of the sample is in the rolling direction.

3. Results

The microstructures were characterized for both the 0Cu and 0.5Cu warm-rolled samples with deformed grains and some in-grain shear bands (Figure 1). However, many more shear bands were present in 0.5Cu sample than in 0Cu sample (Figure 1). Figure 2 shows the textures of 0Cu and 0.5Cu warm-rolled sheets. Here, $L = 0$ and 0.5 represent the surface and middle thickness of the sample, respectively. The warm-rolled texture exhibited a gradient along the thickness in both samples. The dominated texture at the surface of the 0Cu sample was $\{001\}<110>$ with an intensity level of 2.5, and $\{110\}<001>$ with an intensity level of 2.1. The texture at the middle thickness of the 0Cu sample was dominated by $\gamma$ fiber with an intensity level of 3.6 and $\{001\}<110>$ component with an intensity level of 2.9. As shown in Figure 2b, the 0.5Cu sample was much more textured than 0Cu sample.
For the 0.5Cu sample, the texture in surface mainly consisted of Goss component with an intensity level of 6.9, while the main texture in middle thickness was γ fiber and dominated by [111]<112> component with an intensity level of 6.2. Thus, the addition of 0.5 wt. % Cu promoted the formation of shear bands during warm rolling, and strengthened the Goss component at surface layer and the {111}<112> component at the middle thickness of the warm-rolled sheets.

Figure 1. Microstructure of warm-rolled sheets: (a) 0Cu; and (b) 0.5Cu.

Figure 2. Constant $\varphi_2 = 45^\circ$ section of orientation distribution functions (ODFs) at surface ($L = 0$) and middle layer ($L = 0.5$) in warm rolled sheets: (a) 0Cu; and (b) 0.5Cu.

Figure 3 shows the constant $\varphi_2 = 0^\circ$ and $\varphi_2 = 45^\circ$ sections of ODFs of the 0Cu and 0.5Cu sheets after annealing at 900 °C for 10 min. The 0Cu sample exhibited mainly γ and η fibers, while the 0.5Cu sample was dominated by η fiber (especially Goss). Quantitative analysis of the orientation densities along γ fiber ($\Phi = 55^\circ$ and $\varphi_2 = 45^\circ$), η fiber ($\varphi_1 = 0^\circ$ and $\varphi_2 = 0^\circ$) and λ fiber ($\Phi = 0^\circ$ and $\varphi_2 = 45^\circ$) showed that the 0Cu sample was characterized by γ fiber with a strong {111}<112> component, weak η fiber with Goss component, and weak λ fiber with [001]<410> and [001]<310> components (Figure 4). By contrast, the texture in the 0.5Cu sample was dominated by η fiber with a strong peak at Goss; the orientation intensity of γ and λ fibers were extremely weak.
Figure 3. Constant $\phi_2 = 0^\circ$ and $\phi_2 = 45^\circ$ sections in the sheets annealed at 900 °C for 10 min: (a) 0Cu; and (b) 0.5Cu.

Figure 4. The orientation densities along $\gamma$, $\eta$ and $\lambda$ fibers of the sheets annealed at 900 °C for 10 min.
Table 1 summarizes the magnetic induction of the 0.3 mm thickness sheets annealed at 900 °C for 10 min. The $B_8$ and $B_{50}$ values are higher for the 0.5Cu sample (1.37 T and 1.62 T, respectively) than for the 0Cu sample (1.25 T and 1.47 T, respectively).

Table 1. The magnetic properties of the sheets (0.3 mm thickness) annealed at 900 °C for 10 min.

<table>
<thead>
<tr>
<th>Samples</th>
<th>$B_8$/T</th>
<th>$B_{50}$/T</th>
</tr>
</thead>
<tbody>
<tr>
<td>0Cu</td>
<td>1.25</td>
<td>1.47</td>
</tr>
<tr>
<td>0.5Cu</td>
<td>1.37</td>
<td>1.62</td>
</tr>
</tbody>
</table>

4. Discussion

4.1. Effect of Cu on the Formation of Shear Bands

According to the microstructural result of the warm-rolled sheets, the shear band density was indeed higher in the 0.5Cu sample than in the 0Cu sample. It has been shown that the formation of shear bands can be influenced by rolling temperature, strain rate sensitivity and microstructure of the alloys [18–21]. The population of shear bands decreases as the rolling temperature increases. At warm rolling temperatures, the strain rate sensitivity is significantly increased, suppressing inhomogeneous plastic flow and hence shear band formation. A higher value of strain-rate sensitivity ($m$) means that a higher stress is necessary to obtain the same strain. A low strain rate sensitivity will enhance the formation of shear bands and, conversely, a high strain rate sensitivity can suppress their formation within the grains.

Previous study [16] indicated that the addition of 0.5 wt. % Cu could improve the ductility of Fe-6.5 wt. % Si alloy by suppressing the formation of ordered phases in the alloy, and the strain rate sensitivity of the 0.5Cu sample is lower than that for 0Cu sample. Toroghinejad et al. [18] indicated that a material must contain strong [111] and weak [001] components to have good formability. The texture measurements of the warm-rolled sheets show that the intensity of the $\gamma$ fiber texture in 0.5Cu sample is much higher than in the 0Cu sample, and there are some $\alpha$ and [001] textures in 0Cu sample. Therefore, the texture measurement results are consistent with the ductility results. Therefore, a larger number of shear bands will be formed in the 0.5Cu sample than in the 0Cu sample according to the formation mechanism of shear bands. As the rolling temperature of the 0Cu sample and 0.5Cu sample is the same in this study, lower strain rate sensitivity and better ductility will induce a larger number of shear bands for the 0.5Cu sample.

Qaudir et al. [10] found that the in-grain shear bands have a grain orientation dependency, i.e., such shear bands are present in $\gamma$ grains and almost absent in $\alpha$ grains. According to the texture results in this study, the texture of the 0Cu sample was dominated by $\gamma$ fiber and $\alpha$ fiber, while the main texture for the 0.5Cu sample consisted of mainly Goss (the surface) and $\gamma$ fiber (the middle layer), and also the latter sample was more textured than the former sample. Thus, a larger number of shear bands would be expected in the 0.5Cu sample than in the 0Cu sample.

4.2. Effect of Shear Bands on the Nucleation and Growth of $\eta$ Fiber

It is known that magnetization is hardest in the <111> direction but easiest in the <001> direction of iron crystals [22–24]. Thus, the $\eta$ fiber (<001> parallel to the rolling direction) and the $\lambda$ fiber (<001> parallel to the normal direction) are beneficial for magnetic induction, while the $\gamma$ fiber (<111> parallel to the normal direction) is the least favorable for magnetic induction. As the dominating texture after recrystallization was $\gamma$ and $\eta$ fibers in the 0Cu sample, and only $\eta$ fiber in the 0.5Cu sample, the magnetic induction was higher for the 0.5Cu sample than for the 0Cu sample.

To further analyze the texture evolution during recrystallization, the orientation image maps of the partially recrystallized samples were obtained from EBSD measurements (Figure 5). After annealing at 900 °C for 30 s, the nucleation sites in the 0Cu sample were mainly at the boundaries of the
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deformed grains (indicated by circle in Figure 5a), but the recrystallized grains were too coarse to allow identification of the nucleation site in the 0.5Cu sample (Figure 5b). To identify the nucleation site of the 0.5Cu sample, its orientation image map was measured after annealing at 900 °C for only 15 s. In addition to nucleation at grain boundaries, the in-grain shear bands with {111}<112> orientation also acted as nucleation sites (highlighted by arrowed lines in Figure 5c). The grains nucleated at the shear bands grew more quickly than those nucleated at the grain boundaries (Figure 5b,c). Figure 6 summarizes the proportion of γ, η and λ oriented grains in all recrystallized grains observed in Figure 5a,b. In the 0Cu sample, the proportion of γ oriented grains was evidently the highest, which was followed by that of the λ oriented grains (with an area fraction of 27% and 15%, respectively). The area fraction of η oriented grains was less than 5%. For the 0.5Cu sample, the recrystallized grains were dominated by η oriented grains with an area fraction of 25%, whereas the area fractions of the γ and λ oriented grains were only 8% and 6%, respectively.

Figure 5. Orientation image map of partially recrystallized samples: (a) 0Cu, 900 °C × 30 s; (b) 0.5Cu, 900 °C × 30 s; and (c) 0.5Cu, 900 °C × 15 s. The left images are of the normal direction (ND), while the right images are of the rolling direction (RD).

The boundaries of deformed grains and in-grain shear bands will be the nucleation sites of recrystallization, but the η orientation grains will nucleate mainly at the shear bands during recrystallization [25,26]. The schematic diagram in Figure 7 illustrates the recrystallization nucleation of the warm-rolled sheets during annealing processes. The nucleation during the recrystallization...
begins in the shear bands due to the high deformation energy accumulated [27]. The nucleation occurred in the shear bands at the beginning of recrystallization and the new grains grew along the shear band direction, which was at approximately 35° angle to the rolling direction. Most of the grains nucleated on the shear bands had a texture dominated by the η fiber [11,27]. The strong γ and λ textures in the warm-rolled 0Cu sheet resulted in the nucleation of γ and λ oriented grains along the boundaries of deformed grains [11,12], but the low intensity of the shear band in this sample resulted in the lack of the nucleation sites for η oriented grains [28] at the beginning of recrystallization. On the other hand, the high-density of the shear bands in warm-rolled 0.5Cu sample provided plenty of nucleation sites for the η oriented grains, and resulted in the formation of a η fiber dominated texture at the beginning of recrystallization.

![Bar chart showing proportion of γ, η, and λ oriented grains in all recrystallized grains after annealing at 900 °C for 30 s (deviation angle: 15°).](chart)

**Figure 6.** Proportion of γ, η and λ oriented grains in all recrystallized grains after annealing at 900 °C for 30 s (deviation angle: 15°).

![Schematic diagrams showing recrystallization nucleation of warm-rolled sheets during annealing treatment.](diagram)

**Figure 7.** The schematic diagram showing the recrystallization nucleation of the warm-rolled sheets during annealing treatment: shear bands in: 0Cu (a); and 0.5Cu (c) warm-rolled sheets; and the recrystallization nucleation of: 0Cu sample (b); and 0.5Cu sample (d).
The grain orientations at the beginning of recrystallization have significant influence on the final recrystallization texture. In the 0Cu sample, large numbers of $\gamma$ and $\lambda$ oriented grains (nucleated at $\gamma$ and $\lambda$ deformed grains, respectively) were present at the beginning of recrystallization. However, the growth rate of $\gamma$ oriented grains was higher than that of the $\lambda$ oriented grains because the stored energy in the $\gamma$ deformed grains is higher than in the $\lambda$ deformed grains [29,30]. Thus, the $\gamma$ texture dominated the recrystallization microstructure of the 0Cu sample after annealing. For the 0.5Cu sample, the $\eta$ oriented grains (including Goss oriented grains) nucleated at shear bands in $\{111\}<112>$ deformed matrices at the beginning of recrystallization. $\Sigma$19 grain boundaries with high migration rate can form between the nucleated Goss oriented grains and the deformed matrices, which can favor the growth of Goss oriented grains [31–33]. Moreover, the dominant texture in the surface of the warm-rolled 0.5Cu sample was Goss texture. These warm-rolled textures will remain and grow in subsequent annealing processes, which will enhance the $\eta$ fiber (especially Goss) after annealing and lead to $\eta$ recrystallization texture with a peak at Goss with improved magnetic properties.

5. Conclusions
(1) The addition of 0.5 wt. % Cu promoted the formation of shear bands after warm rolling, and strengthened the $\{110\}<001>$ texture at surface layer and $\{111\}<112>$ texture in the middle layer.
(2) The shear bands in $\{111\}<112>$ oriented grains acted as the nucleation sites of $\eta$ oriented grains and hence promoted the growth of Goss oriented grains.
(3) After recrystallization, the dominant texture in the 0.5Cu sample consisted of mainly $\eta$ fiber with a peak at Goss, while the texture of the 0Cu sample was characterized by a combination of $\gamma$, $\eta$, and $\lambda$ fibers.
(4) The 0.5Cu sample had higher magnetic induction than the 0Cu sample due to the formation of relatively stronger $\eta$ fiber texture through the thickness.

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Conflicts of Interest: The authors declare no conflict of interest.

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