Article

Field Water Balance Closure with Actively Heated Fiber-Optics and Point-Based Soil Water Sensors

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Abstract: While traditional soil water sensors measure soil water content (SWC) at point scale, the actively heated fiber-optics (AHFO) sensor measures the SWC at field scale. This study compared the performance of a distributed (e.g., AHFO) and a point-based sensor on closing the field water balance and estimating the evapotranspiration (ET). Both sensors failed to close the water balance and produced larger errors in estimated ET (ETε), particularly for longer time periods with >60 mm change in soil water storage (∆SWS), and this was attributed to a lack of SWC measurements from deeper layers (>0.24 m). Performance of the two sensors was different when only the periods of <60 mm ∆SWS were considered; significantly lower residual of the water balance (Rε) and ETε of the distributed sensor showed that it could capture the small-scale spatial variability of SWC that the point-based sensor missed during wet (70–104 mm SWS) periods of <60 mm ∆SWS. Overall, this study showed the potential of the distributed sensor to provide a more accurate value of SWS at field scale and to reduce the errors in water balance for shorter wet periods. It is suggested to include SWC measurements from deeper layers to better evaluate the performance of the distributed sensor, especially for longer time periods of >60 mm ∆SWS, in future studies.

Keywords: soil water balance; actively heated fiber-optics; soil water storage

1. Introduction

Changes in soil water affect crop growth, grain yield and other ecological processes such as salinity, nutrient transformation, and emission of greenhouse gases (CO₂, CH₄ and, N₂O) from the soil. An accurate estimation of the ∆SWS is also important for improving the field water balance closure, in addition to the measurements of other components of the water balance, such as precipitation and ET. Improving knowledge about the soil water balance at the field scale is important to be able to understand the hydrological processes necessary to optimize water management practices. In irrigation scheduling, an accurate water balance is required to determine the timing and amount of water to be added. Under rainfed systems, the water balance is a powerful tool to predict the crop response under different climatic and management scenarios.

The soil water balance requires data on its components. While precipitation is commonly measured, and methods exist to determine ET at the field scale (e.g., eddy covariance) [1], the ∆SWS at this scale has been more difficult to obtain. ∆SWS can be determined directly using weighing lysimeters or soil water sensors. Weighing lysimeters are expensive and, although accurate, are difficult to manage and afford little replication at the field scale. Direct soil water measurement methods (e.g., gravimetric) are accurate, but are typically destructive and time/labor-intensive. Traditional point-based soil water sensors such as TDR, and neutron or capacitance probes have been used to estimate ∆SWS and to improve the soil water balance estimations [2–4]. However, traditional point-based sensors

measure SWC at point scale (<1 m²) and could lead to high uncertainty in estimating the overall ∆SWS at field scale due to the spatial variability of soil water. To obtain an accurate estimate of the overall ∆SWS through the depth of the control volume requires a sufficient number of measurement points distributed within the area (e.g., field). Impractically, a large number of point-based sensors and/or access tubes are required to obtain an accurate estimate of the overall ∆SWS at the field scale. Soil water content at larger scales can be estimated using satellite-based techniques, such as passive or active microwave sensors [5,6], but spatial resolutions are typically coarse and overpass times infrequent as compared to the spatiotemporal variability of soil water at the field scale. Another challenge of remote sensing is that only the surface soil water (top 5 cm of the soil profile) can be estimated [7–9], which hampers the estimation ∆SWS in the whole profile. One approach to addressing the scale gap in soil water measurement is the use of sensors, which could provide accurate soil water measurements from scales representing small plots up to the field. Several sensing techniques have emerged to measure SWC at field scale including cosmic ray probes [10–12], electromagnetic induction sensors (EMI) [13,14], ground penetrating radar (GPR) [15,16], electrical resistivity imaging (ERI) [17,18], global positioning system (GPS) reflectometry [19], and actively heated fiber-optics (AHFO) [20–24]. Among these sensing techniques, the AHFO is a relatively new sensor that provides spatially distributed SWC measurements along a fiber-optic cable (e.g., 0.5 m spatial resolution). Therefore, AHFO could provide a sufficient number of SWC measurements through time and be expected to provide an accurate estimate of the overall ∆SWS within the field. To date, calibration and validation of the AHFO technique have been done at laboratory [20–22,25,26] and field [23,24,27] scales. To our knowledge, no studies have compared ∆SWS determined using AHFO and point-based sensors with the ∆SWS calculated from a simple water balance at the field scale.

Good knowledge of the soil water balance at small field to plot scales is necessary to understand the water and solute behaviour in cultivated soils. Evaluating soil water and solute fluxes in cultivated soils is important for irrigation water management and understanding the response of the system due to various management practices. For example, soil water balance involves the quantification of all water inputs and outputs at the site in order to determine the how much water is being used by plants and how much water is being lost in the vadose zone. Therefore, understanding soil water dynamics by means of soil water balance is essential for irrigation water management. Furthermore, the relation between ET and SWC is an important parametrization in land surface models [28,29] and in most cases have been investigated using eddy covariance (EC) measurements of ET combined with SWC measurements at point scale. Several studies, however, have shown that accounting for the spatial variability of soil water is important to quantify the relationship between ET and soil water accurately [30–32]; AHFO SWC measurements could be useful to improve the accuracy of such relationships at the field scale. In this study, first, we compare the performance of a distributed soil water sensor (i.e., AHFO) and a point-based soil water sensor on closing the water balance; and second, we compare ET estimated from both sensors with the ET measured using the EC technique in an agricultural field under corn production in Eastern Canada over a cropping season.

2. Materials and Methods

2.1. Study Site

The study site was a 4.2 ha experimental corn field located near Coteau-du-Lac, Québec, Canada (Figure 1a) approximately 60 km west of Montréal. The soil is classified as a Planosol (WRB) (Soulanges very fine sandy loam) [33], has a mean depth of 0.50–0.90 m and overlies clay deposits from the Champlain Sea. The field has a flat topography, with an average slope of less than 0.5% [34]. The study site consisted of three blocks (A, B and C) and each block comprised eight subplots (15 m × 75 m) (Figure 1b). In the center of each subplot, a tile drain had been installed at 1.0 m depth. These drains discharge into two buildings located on the northern side of the field (Figure 1b). Heating
and ventilation help to keep a thermally stable environment inside each building which facilitates year-round measurement of drainage volume.

Figure 1. (a) The location of the study area, approximately 60 km west of Montreal, (b) the study area consists of three main blocks A, B and C. Blue and green rectangles within the main blocks are subplots (15 × 75 m) of free drainage (FD) and controlled drainage (CD), respectively. Two water houses facilitate the measurement of drainage volume from each subplot and (c) the fiber-optic cable configuration in the field which shows a cable connected to the DTS instrument starts from water house I and runs through two subplots at three depths (0.04, 0.12 and 0.20 m), red triangles show the locations of the point-based sensors used for calibration, validation, and point-based measurements. The distributed soil water sensor represents only the fiber-optic cable transects installed within the two sub-plots.

2.2. Soil Water Measurement

Soil water measurements were obtained using two sensor types, namely, a point-based sensor (5TE, Decagon Inc., Pullman, Washington, USA) and a distributed soil water sensor developed using the AHFO technique. The point-based sensor measured SWC every five min while the distributed soil water sensor measured SWC every six hours during the experimental period. The distributed soil water sensor (i.e., AHFO) measured SWC every 0.5 m along six, 64 m long parallel cable transects at the three depths covering 768 locations of the experimental site. The point-based sensors measured SWC at four locations and three depths (i.e., 0.04, 0.12 and 0.20 m) (Figure 1c). Soil water content measured from both sensing techniques were averaged temporally (i.e., to daily scales) and spatially (N = 3 for 5TE and N = 768 for AHFO) for soil water balance calculations. Soil water data from only three 5TE sensor locations were used to calculate the spatially averaged SWC due to a technical problem at one location. \( \Delta SWS \) was calculated using the volumetric soil water contents \( (\theta_v, \text{mm}^3 \text{mm}^{-3}) \) measured at respective depths using

\[
\Delta SWS = \frac{\sum_{i=3}^{3} [\theta_v(z_i) - \theta_v(z_{i+1})] \times \Delta z_i}{\Delta t}
\]

where \( \theta_v \) measurements were integrated over each soil layer \( z_i \) (mm) for a given time interval \( \Delta t \) (days) to obtain \( \Delta SWS \). There were three layers: (1) 0–0.08 m, (2) 0.08–0.16 m and (3) 0.16–0.24 m. It was assumed that each soil layer was homogenous and that \( \theta_v \) measured in the middle of each layer (i.e., 0.40, 0.12 and 0.20 m) was representative of the layer. Therefore, an integration interval \( (\Delta z_i) \) of 0.08 m was used for each depth and SWS was calculated to a 0.24 m depth from the surface of the soil.
2.3. Development of the Distributed Soil Water Sensor Using Actively Heated Fiber-Optics

The AHFO technique is based on the distributed temperature sensor (DTS), which measures the temperature at high spatial (<1 m) and (1 s) resolutions along a fiber-optic cable, potentially exceeding 10 km in length. More details on the development, calibration, and validation of the AHFO technique can be found in Vidana Gamage et al., [27]. However, a brief summary of the development, calibration, and validation of the AHFO technique is presented here. A DTS (Linear Pro series, AP Sensing, Germany), consisting of two channels with a maximum measurement range of 4 km was used in this study. The AHFO technique applies an electrically generated heat pulse to the metal sheath of the fiber-optic cable and the resulting temperature change (thermal response) during (heating phase) or after (cooling phase) the heat pulse is related to the water content of the soil using either empirically or physically-based equations. 240 volts were applied to each cable section of 147.3 m long (three cable sections per depth) to produce heat pulses of 7.28 W m\(^{-1}\). Heat pulses were sent for five minutes duration at every six hours during a day starting from 12:00 a.m. on the morning of 22 July 2016 to the 6:00 p.m. on the evening of 17 October 2016. The DTS recorded the thermal response (i.e., temperature increase) every 30 s (temporal) and 0.5 m sampling interval (spatial) of the fiber-optic cable during the heating. The integral of the cumulative temperature increase (\(T_{\text{cum}}\)) [7] during a heat pulse was calculated at each point of the fiber-optic cable using

\[
T_{\text{cum}} = \int_{0}^{t_0} \Delta T \, dt
\]

where \(T_{\text{cum}}\) is the integral of the cumulative temperature increase (°C s) during the total time of integration \(t_0\) (s) at a given point of the cable, \(\Delta T\) is the DTS recorded temperature change from the pre-pulse temperature (°C). In this study, the average temperature calculated over five minutes prior to each heat pulse was used as the pre-pulse temperature. This average was subtracted from the temperature during the pulse to obtain the temperature increase, \(\Delta T\). \(T_{\text{cum}}\) was then calculated as the sum of the values obtained by multiplying \(\Delta T\) by the time interval (30 s) between measurements. \(T_{\text{cum}}\) was normalized by power intensity (q) of 7.28 W m\(^{-1}\) as \(T_{\text{cum}, N}\) using

\[
T_{\text{cum}, N} = \frac{T_{\text{cum}}}{q}
\]

\(T_{\text{cum}, N}\) is a function of soil thermal properties such as the thermal conductivity; higher thermal conductivity (high SWC), will lead to a higher rate at which the heat is conducted away from the cable resulting in a low \(T_{\text{cum}, N}\) at a given point on the cable. Depth-specific empirical calibration relationships between the \(T_{\text{cum}, N}\) and SWC were developed using the \(T_{\text{cum}, N}\) and SWC data collected at reference cable locations. Independent SWC data measured using nine calibrated 5TE soil moisture sensors (Decagon Devices, Pullman, WA, USA) were used to develop the calibration and validation relationships. Root mean square error (RMSE) was calculated to obtain the averaged predictive accuracy. Soil water content at each 0.5 m length of the cable transects was subsequently obtained from the \(T_{\text{cum}, N}\)-SWC calibration relationships at respective depths.

2.4. Weather and Drainage Data

Daily total precipitation (\(P\)) data measured at a weather station located about 500 m from the experimental site were used for the water balance calculations. Evapotranspiration (\(ET\)) was measured on site at 30 min resolution using the EC technique [1]. The EC system consisted of a three-dimensional sonic anemometer (CSAT-3, Campbell Scientific, Edmonton, Canada) and an open-path infrared gas analyzer (IRGA; LI-7500A, LI-COR, Lincoln, NE, USA). All data were recorded at 10 Hz via an analyzer interface unit (LI-7550, LI-COR Biogeosciences, Lincoln, NE, USA). The \(ET\) data were summed to obtain the daily \(ET\). Drainage outflows were measured at the outlet of each tile drain in the control
buildings, using tipping buckets. Each tipping bucket has a capacity of 1 L and is connected to a DAQ computer that logged cumulative outflows. Each sub-plot had one outlet, and individual daily drainage flows were used from each subplot.

2.5. Soil Water Balance

Water balance in the root zone for a given time period (Δt) is given by

\[ P + I - ET - R - D = \Delta SWS + R_e \]

where \( P \) and \( ET \) are as defined previously, \( I \) is the amount of irrigation water applied, \( R \) is surface runoff, \( D \) is drainage below the root zone, \( \Delta SWS \) is change in soil water storage measured by distributed or point-based soil water sensors within 0.24 m depth and \( R_e \) is the residual component. \( R \) was assumed to be negligible due to the flat topography of the study area and there was no irrigation during the study period. All components are expressed in units of length (mm).

The residual component reflects the lack of water budget closure and represents the sum of the lateral flows, SWS from the deeper layers (>0.24 m) and measurement errors of the different water balance components. Because the \( \Delta SWS \) was only estimated for the top 0.24 m depth for both sensor types, while the drainage below the root zone (\( D \)) was measured at a greater depth (0.90 m), the \( \Delta SWS \) from both sensor types will likely be underestimated, resulting in an increased \( R_e \). However, since both sensors should suffer from the same lack of depth information, the sensor which minimized \( R_e \) from both sensor types would be used to calculate the \( \Delta SWS_5TE \) and \( \Delta SWS_AHFO \).

\[ R_e = P - ET - D - \Delta SWS \]

was considered to provide the best field-scale estimation of SWS.

For both point-based (\( N = 3 \)) and distributed (\( N = 768 \)) sensors, spatially averaged \( \theta_e \) were used to calculate the \( \Delta SWS \) using Equation (1). The \( \Delta SWS \) calculated from the point-based and distributed sensing techniques were denoted as \( \Delta SWS_{5TE} \) and \( \Delta SWS_{AHFO} \), respectively. The \( \Delta SWS \) was also calculated from the simple water balance (using components of the left side of Equation (4)) and denoted as \( \Delta SWS_{WB} \). In all cases, \( \Delta SWS \) was calculated for the entire measurement period (2.5 months) and subsets ranging from days to weeks (Table 1). The agreement between \( \Delta SWS_{WB} \) and \( \Delta SWS_{5TE} \) or \( \Delta SWS_{AHFO} \) was assessed by the correlation coefficient (\( r \)). Furthermore, the difference between \( \Delta SWS \) calculated from each sensor (i.e., \( \Delta SWS_{5TE} \) or \( \Delta SWS_{AHFO} \)) and \( \Delta SWS_{WB} \) was calculated (using Equation (5)) as \( R_e \) and is presented in Table 1.

Table 1. Components of the water balance for each time period and the residual component and relative reduction in error (RRE %) calculated from the change in SWS from distributed (i.e., AHFO) and from point-based (i.e., 5TE) sensors.

<table>
<thead>
<tr>
<th>Period (2016)</th>
<th>Observations (mm)</th>
<th>Residual (mm)</th>
<th>RRE (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>( P )</td>
<td>( ET )</td>
<td>( D )</td>
</tr>
<tr>
<td>22 July–14 August</td>
<td>125.8</td>
<td>174.6</td>
<td>4.3</td>
</tr>
<tr>
<td>22 July–18 August</td>
<td>165.4</td>
<td>197.2</td>
<td>4.4</td>
</tr>
<tr>
<td>22 July–25 August</td>
<td>188.4</td>
<td>235.0</td>
<td>4.4</td>
</tr>
<tr>
<td>22 July–31 August</td>
<td>219.5</td>
<td>268.4</td>
<td>4.4</td>
</tr>
<tr>
<td>22 July–4 September</td>
<td>219.5</td>
<td>292.0</td>
<td>4.4</td>
</tr>
<tr>
<td>22 July–12 September</td>
<td>219.5</td>
<td>332.4</td>
<td>4.4</td>
</tr>
<tr>
<td>23 August–25 August</td>
<td>1.0</td>
<td>15.2</td>
<td>0.0</td>
</tr>
<tr>
<td>1 September–3 September</td>
<td>0.0</td>
<td>17.0</td>
<td>0.0</td>
</tr>
<tr>
<td>24 August–1 September</td>
<td>32.1</td>
<td>46.9</td>
<td>0.0</td>
</tr>
<tr>
<td>20 August–12 September</td>
<td>54.1</td>
<td>125.3</td>
<td>0.0</td>
</tr>
<tr>
<td>9 August–11 August</td>
<td>23.0</td>
<td>26.5</td>
<td>0.0</td>
</tr>
<tr>
<td>20 August–31 August</td>
<td>54.1</td>
<td>61.3</td>
<td>0.0</td>
</tr>
<tr>
<td>25 August–2 September</td>
<td>32.1</td>
<td>46.4</td>
<td>0.0</td>
</tr>
</tbody>
</table>

\( P = \) precipitation, \( ET = \) Evapotranspiration, \( D = \) Drainage, \( WB = \) water balance calculated from simple water balance and \% RRE: percentage relative reduction in \( R_e \).
In addition to the comparison of ΔSWS_AHFO and ΔSWS_5TE to ΔSWS_WB, ΔSWS_AHFO and ΔSWS_5TE were used to estimate the evapotranspiration (ET*) using

$$ET^* = P - D - \Delta SWS$$  \hspace{1cm} (6)

$ET^*$ is the estimated evapotranspiration either using the ΔSWS_AHFO or ΔSWS_5TE and $P$ and $D$, and is as defined previously. ETc error in ET estimation can be estimated using

$$ET_c = ET - ET^*$$  \hspace{1cm} (7)

The soil water sensing technique that provided the lowest $ET_c$ was considered to provide the closest estimate of $ET$ as compared with that measured using EC.

Independent two-sample Wilcoxon test (a non-parametric independent two-sample test) was conducted to test if there was any significant difference between the $R_c$ means and between the $ET_c$ means estimated from the two sensing techniques at $p < 0.05$ probability level. The relative reduction in error (RRE) was calculated as the difference between $R_c$ for the distributed and point-based sensors (for water balance) and expressed as a percentage of the computed ΔSWS_WB.

3. Results and Discussion

3.1. Calibration and Validation of the Soil Water Sensors

The relationship between $T_{cum\_N}$ and SWC was stronger for all three depths (0.05 m: $R^2 = 0.90$; 0.10 m: $R^2 = 0.91$; 0.20 m: $R^2 = 0.93$), with RMSEs of 0.08, 0.12, and 0.18, respectively (Figure 2). Calibration relationships showed a similar shape for all the depths despite the differences in the maximum and minimum SWC values. The sensitivity of $T_{cum\_N}$ was relatively low in dry soil (<20%), and it started to increase at an increasing rate, with the rate decreased after reaching a SWC between 35% and 40% for all the depths (Figure 2). These results are comparable with the findings by Sayde et al. [21], who observed a lower sensitivity of $T_{cum\_N}$ at higher water contents. However, most of the SWC values measured during the experimental period fell within the range of 15–35%, while only a few values were found between 35 and 40%. Therefore, the distributed soil water sensor could measure the SWC accurately across a wider SWC range. Root mean square error of calibrated point-based sensors was 2%, which suggested a good measurement accuracy. In comparison to the calibrated point-based sensors (gravimetrically), the distributed water sensor showed predictive accuracies of RMSE of 3.3, 2.8 and, 3.7% for 0.04, 0.12 and 0.20 m depths, respectively.

![Figure 2](image-url)  \hspace{1cm} Figure 2. Calibration relationships between soil water content and $T_{cum\_N}$ (a) 0.04 m, (b) 0.12 m, and (c) 0.20 m depths, respectively.

3.2. Comparison of the Distributed Sensor with the Point-Based Sensor

Overall, both point-based and distributed sensors failed to close the water balance, and underestimated the ΔSWS_WB for the selected time periods (Figure 3a), which was primarily due to a lack of SWC measurements from layers >0.24 m. Therefore, we focused the discussion mainly on a...
comparison of the residual, $R_c$ between the two sensors and the magnitude of the RRE%. Because the absolute values of $R_c$ estimated from distributed sensor were always lower than those of the point-based sensor, a larger RRE% indicated a better performance of the distributed sensor for estimating the overall $\Delta SWS$. The residual component, $R_c$, represented the sum of the lateral flows, SWS within layers beneath the measurement zone (>0.24 m), and any measurement errors of the different water balance components (i.e., $ET$, $P$, $D$, and soil water content). Estimates of $P$ can have a wide range of error, depending on the gauge placement, gauge spacing, and areal averaging technique [35]. In addition to the errors associated with the gauges, a considerable error can result from the ambient wind speed [36,37]. Though $ET$ was estimated at high temporal resolutions using the EC technique, the footprint of the measurement is not fixed in time [38,39], and this could introduce an additional error. The vertical plastic barriers between the plots were installed in 1992 and extended to 1.5 m into the ground. Some seepage between plots can occur below this point, as the soil at 1.5 m depth is not impermeable. Therefore, some errors associated with estimates of $D$ could also contribute the $R_c$ component. However, $D$, $ET$ and $P$ contribute the same error for the estimations of water balance using each of the soil water sensing techniques. The underestimation of SWS from the lack of deep measurements is also similarly common between the sensors. Therefore, differences resulting between the two $R_c$ estimates are due to the water sensing techniques.

The correspondence between the $\Delta SWS_{AHFO}$ and $\Delta SWS_{WB}$ was strong for the $\Delta SWS$ flux <60 mm range, but the discrepancy was higher when the $\Delta SWS$ flux was >60 mm (Figure 3a). In contrast, the point-based sensor consistently underestimated the $\Delta SWS_{WB}$ and showed a higher discrepancy (Figure 3a). The poor agreements between $\Delta SWS_{AHFO}$ and $\Delta SWS_{WB}$ were attributed to three time periods where $\Delta SWS_{WB}$ was above 60 mm (Figure 3a). Large $P$ events that occurred during these periods likely caused the infiltration front to penetrate beyond 0.24 m depth and this, therefore, was not captured by the either the distributed or point sensor. For example, the highest $\Delta SWS$ of 117 mm was reported for the whole experimental period from 22 July to 12 September 2016, and that period included two $P$ events of >20 mm. Therefore, a smaller difference of $R_c$ (23 mm) between the two sensors was observed during this period (Table 1). However, the $\Delta SWS_{AHFO}$ showed an excellent agreement with $\Delta SWS_{WB}$ after removing the three periods from the correlation analysis; $r$ between $\Delta SWS_{AHFO}$ and $\Delta SWS_{WB}$ increased to 0.95, while $r$ between $\Delta SWS_{STE}$ and $\Delta SWS_{WB}$ only increased to 0.70 (Figure 3b). The results clearly showed that the distributed sensor outperformed the point-based sensor when there was a minimal loss of water to deeper layers (>0.24 m).

![Figure 3](image-url)

**Figure 3.** (a) The change in soil water storage computed by the simple water balance ($\Delta SWS_{WB}$) and spatially averaged change in soil water storage measured by the point-based sensors ($\Delta SWS_{STE}$), and measured by the AHFO sensor ($\Delta SWS_{AHFO}$) (N = 12); and (b) as in (a), after removing the three periods with >60 mm $\Delta SWS$. The correspondences between the $\Delta SWS_{AHFO}$ and $\Delta SWS_{WB}$ was strong for the $\Delta SWS$ flux <60 mm range, but the discrepancy was higher when the $\Delta SWS$ flux was >60 mm (Figure 3a).
The strength of the agreement between each sensor-measured ΔSWS and ΔSWS_WB during the periods of <60 mm ΔSWS mainly depended on the ability of a particular sensor to capture the spatial variability of SWC and to provide a more accurate estimate of ΔSWS at the field scale. The coefficient of variation (CV) of SWC measured by the distributed sensor was consistently higher than that of the point-based sensors (Figure 4), thus indicating that the distributed sensor captured more spatial variability of SWC than that of the point-based sensors during the whole experimental period. According to Blöschl and Sivapalan [40], the variability of the SWC could be affected by the three types of scales: spacing, support, and extent. Spacing refers to the distance (or time) between the measurements, support to the averaged volume or area (or time) of a single measurement, and extent to the overall coverage of the measurements (in space or time). In this study, the spacing between the point-based sensors was larger (26–46 m) compared to that of the distributed sensor (0.5 m), and apparently, the point-based sensors failed to capture the small-scale variability in the field throughout the experimental period and contributed to the difference between the CVs for distributed and point-based sensors. A larger difference between the CVs for distributed and point-based sensor (shaded area in Figure 4) during the wetter period (after 10 August) indicated that the distributed sensor captured a substantial amount of small-scale variability in wetter periods. Both sensors captured the spatial variability of SWC during the drier period while the distributed sensor likely gave more accurate magnitude during this period (Figure 4).

![Figure 4](image-url)  
*Figure 4. Temporal changes of the coefficient of variation (CV) of soil water content measured by the distributed sensor technique and the point-based sensor. The coefficient of variation was calculated using the spatial mean and the spatial standard deviation of measured soil water contents of distributed sensor (N = 768) and point-based sensor (N = 3). Dark grey colored bars show the rainfall distribution (mm, in the right Y-axis) during the time period. The shaded area shows the difference between the two CV’s of soil water content measured by the two sensors.*

When the time period considered for water balance calculation was longer, ΔSWS at deeper layers (>0.24 m) caused by either wetting (by P) or drying (by ET) was substantial, and therefore, this resulted in a relatively larger R_e. For example, time periods from 22 July to 12 September and 22 July to 4 September showed larger R_e,s for both sensor types (Table 1). ET influenced ΔSWS at deeper (>0.24 m) layers significantly at the beginning and intense P events (>20 mm) also caused a substantial ΔSWS at deeper layers in the middle and end of the periods. When shorter time
periods were considered, \( R_e \)'s of both sensor types were relatively smaller than that of the longer time periods, but substantial differences between the \( R_e \) of point-based sensor and that of the distributed sensor were only observed for relatively wet time periods (Table 1). Therefore, the distributed sensor showed a better performance on estimating overall \( \Delta SWS \) for shorter wet periods. For example, the highest RREs of 62\%, 50\%, and 42\% were reported for the periods of 24 August to 1 September, 23 August to 1 September, and 23 August to 25 August, respectively (Table 1). Despite the shorter time period, the lowest RRE of 8\% was reported for the drier period from 22 July to 14 August (Table 1), which indicated that the distributed sensor showed a little improvement in reducing the \( R_e \). These results indicated that the distributed sensor outperformed the point-based sensor, by capturing more small-scale spatial variability of soil water content, particularly during the shorter wet periods.

Results of the two-sample Wilcoxon test statistically verified these observations. Results showed no significant difference between the median \( R_e \) of the point-based sensor and that of the distributed sensor (\( n = 14 \) and \( p = 0.11 \)) when all the time periods were considered. However, the median \( R_e \) of the point-based sensor was significantly higher than that of the distributed sensor (\( n = 7 \) and \( p = 0.03 \)) when only the shorter wet periods were included (Figure 5).

\[ \text{Figure 5. Box and whisker plots showing the distribution of the residual of the water balance, } R_e (\text{mm}) \text{ for each sensing technique. Orange plots include } R_e \text{ values from all the time periods (N = 14), and light blue plots include only the wetter time periods (N = 7). The horizontal line and the cross within a box indicate the median and mean } R_e \text{, respectively. Boundaries of the box indicate the 25th and 75th percentile and whiskers indicate the maximum and the minimum values of } R_e. \]

\subsection*{3.3. Comparison of Evapotranspiration Estimates}

Overall, both point-based and distributed sensors underestimated the \( ET \) (Table 2), likely due to the lack of SWC measurements from deeper layers which was similarly common between the two sensing techniques. Therefore, any differences in the \( ET_e \) or cumulative \( ETs \) between the two sensing techniques could be attributed to the performance of the two soil water sensing techniques. \( ET_e \) ranged from 115 mm to 4.6 mm and 113 mm to \(-2.7 \) mm for the point-based and distributed sensing techniques, respectively. The two sensing techniques showed no difference in \( ET^* \) for the
period from 22 July to 12 August, and both sensing techniques underestimated ET by 115 and 113 mm, respectively (Table 2). Furthermore, the discrepancy between the cumulative ET of the distributed sensor and that of the point-based sensor was negligible during the early dry period, while cumulative ETs of both sensors showed a least match to the EC measured ET during this period (Figure 6). Both sensors failed to capture the amount of water that was removed from the deeper soil layers (>0.24 m) by the ET during the early dry period from 22 July to 12 August, and this resulted in a larger difference between the cumulative ETs of sensors and cumulative ET measured by EC (Figure 6). There was a smaller difference in the CVs of SWC measured by both sensors during the early dry period (Figure 4), and this likely resulted from a lack of small-scale variability of SWC in dry soil. Therefore, the distributed sensor showed a poor performance in estimating ET during the early dry period.

### Table 2. Components of the water balance and evapotranspiration estimated using change in soil water storage measured from distributed and point-based sensors and the respective error in ET estimations for selected time periods.

<table>
<thead>
<tr>
<th>Period (2016)</th>
<th>Observations (mm)</th>
<th>Estimations (mm)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>P</td>
<td>ET</td>
</tr>
<tr>
<td>22 July–12 August</td>
<td>54.8</td>
<td>171.0</td>
</tr>
<tr>
<td>22 July–14 August</td>
<td>125.8</td>
<td>174.6</td>
</tr>
<tr>
<td>22 July–18 August</td>
<td>165.4</td>
<td>197.2</td>
</tr>
<tr>
<td>22 July–25 August</td>
<td>188.4</td>
<td>235.0</td>
</tr>
<tr>
<td>22 July–31 August</td>
<td>219.5</td>
<td>268.4</td>
</tr>
<tr>
<td>22 July–4 September</td>
<td>219.5</td>
<td>292.0</td>
</tr>
<tr>
<td>22 July–12 September</td>
<td>219.5</td>
<td>324.4</td>
</tr>
<tr>
<td>9 August–11 August</td>
<td>23.0</td>
<td>26.5</td>
</tr>
<tr>
<td>23 August–25 August</td>
<td>1.0</td>
<td>15.2</td>
</tr>
<tr>
<td>24 August–1 September</td>
<td>32.1</td>
<td>46.9</td>
</tr>
<tr>
<td>20 August–2 September</td>
<td>54.1</td>
<td>125.3</td>
</tr>
<tr>
<td>20 August–31 August</td>
<td>54.1</td>
<td>61.3</td>
</tr>
<tr>
<td>25 August–2 September</td>
<td>32.1</td>
<td>46.4</td>
</tr>
<tr>
<td>1 September–3 September</td>
<td>0.0</td>
<td>17.0</td>
</tr>
</tbody>
</table>


Performance of the distributed sensor in estimating the ET was better and more noticeable for shorter wet periods than the longer periods (Table 2). For example, ETc of distributed sensor decreased by approximately three and four times, respectively, for the periods of 24 August to 01 September and 23 August to 25 August compared to the ETc of the point-based sensor. The cumulative ET of the distributed sensor also exhibited the similar pattern; the cumulative ET of the of the distributed sensor showed a relatively close match to the cumulative ET measured by the EC after 14 August. However, the ETc of the distributed sensor showed no substantial differences to that of the point-based sensor for longer time periods (e.g., from 22 July to 12 September and 22 August to 12 September) (Table 2). The discrepancy between the cumulative ET’s of the two sensors and the cumulative ET measured by EC was also high towards the end of the experimental period (Figure 6). When the time period was longer, ΔSWS at deeper layers, which was brought by P and ET, could be significant, and this might have contributed to larger ETc. These results can be further examined by statistically comparing the medians of ETc of the two sensing techniques including all the time periods as well as including only shorter wet periods. The median ETc of the point-based sensor showed no significant difference from that of the distributed sensor (n = 15 and p = 0.07) when all the time periods were considered. However, the inclusion of only the shorter wet periods resulted in a significant difference between the median ETc of the point-based sensor and that of the distributed sensor (n = 7 and p = 0.01) (Figure 7). Overall, the results from individual time periods and two-sample t-test showed a better performance of the distributed sensor during the shorter wet periods. Soil water content measurements from deeper layers (>0.24 m) are necessary to compare the performance of the two sensors for longer time periods.
Because the accuracy of the $ET^*$ depended on an accurate average value of $\Delta SWS$ obtained from the whole soil profile. Results of $ET$ estimations reinforced the fact that the distributed sensor captured more variability in wetter soils and reduced $ET_e$ significantly compared to that of the point-based sensor during the shorter periods.

![Cumulative ET measured using eddy covariance (solid black line) and cumulative rainfall (black dotted line) during the experimental period. Solid circles (point-based) and open circles (distributed) sensors show the cumulative ET values (from 22 July to selected dates) estimated using the measured $\Delta SWS$ (see Equation (4)).](image)

The distributed soil water sensor (i.e., AHFO) measured SWC at high spatial resolutions (e.g., 0.50 m) and captured more small-scale variability of SWC than that of few point-based sensors. A larger difference between the CVs of the two sensors in wetter periods clearly indicated a dominance of small-scale variability in wet soils, and this was captured by the distributed soil water sensor. The scale of the spatial variability of SWC mainly depends on the scale of the controlling processes. Under wet conditions, the variability is mainly controlled by small-scale variability in hydraulic conductivity and porosity at field scale, while the spatial variability of SWC in dry soils is largely influenced by large-scale processes such $ET$ [41–44]. However, the scope of this study was only to compare the performance of the two sensors on closing the water balance. Hence, more analysis is needed to identify the controls of the variability and their season dependency.
Figure 7. Box and whisker plots showing the distribution of the $ET_\varepsilon$ (mm) for each sensing technique. Orange colored plots include $ET_\varepsilon$ values from all the time periods ($N = 15$) and light blue colored plots include only the wetter time periods ($N = 7$). The horizontal line and the cross within a box indicate the median and mean $ET_\varepsilon$, respectively. Boundaries of the box indicate the 25th and 75th percentile and whiskers indicate the maximum and the minimum values of $ET_\varepsilon$.

4. Conclusions

In this study, we compared the performance of a point-based (5TE) and a distributed soil water sensor (AHFO) on closing the field water balance and estimating the $ET$ in a corn production agricultural field of eastern Canada. The $\Delta SWS$ determined using each sensor was compared with the $\Delta SWS$ calculated from simple water balance at field scale. The $\Delta SWS$ determined using the two sensors was also used to estimate the $ET$ and was compared with $ET$ measured using eddy covariance. Results of this study emphasized the need for SWC measurements from deeper layers (>0.24 m) to close the water balance and accurately estimate the $ET$, particularly for longer time periods. However, significantly lower $R_e$ and $ET_\varepsilon$ of the distributed sensor showed that it could capture more small-scale spatial variability of SWC and outperform the point-based sensor in shorter wet periods. Overall, this study showed the potential of the distributed soil water sensor to provide a more accurate overall value of SWS at field scale and to reduce the errors in water balance. The results of this study also highlighted the need to consider the change in the size of the sampling domain through time in soil water balance studies. It is suggested to include the SWC measurements from deeper layers to better evaluate the performance of the distributed sensor, especially for the longer periods of larger change in soil water storage (i.e., >60 mm) in future studies.

Author Contributions: D.N.V.G. and A.B. conceived and designed the experiment; D.V.G. performed the experiment and analyzed the data and wrote the manuscript. A.B. and I.B.S. contributed to scientific advising and provided a substantial input to improve the paper.

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Conflicts of Interest: The authors declare no conflict of interest.

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